Oops!

How I Goofed Simulating Overunity Circuits on a 32-bit Computer...

© Sunday, May 1st 2022 ~ Vinyasi

Sorry about my previous five years of circuit simulations. They were designed on various 32-bit computers which made them unstable and it was very easy to produce overunity. Yet, they lacked credibility and put into question whether they were buildable. Now, I'm working on a 64-bit computer. I get the distinct impression that Micro-Cap electronic simulator...

https://www.spectrum-soft.com/

...was designed and intended to run on a computer of this type. A 64-bit computer simulation, in the Micro-Cap variety of Berkeley SPICE, is much more stable.[1] This makes it very unlikely to produce overunity and more likely to produce a comatose circuit simulation unless I keep the circuit very simple and continue to adhere to various design principles, such as (but not limited to):

1 https://www.youtube.com/watch?v=s1WnjQpuexU - The Difference Between 32 Bit and 64 Bit Systems (Old Edition - New Video in Description!) - Computer Clan

1. Keep the input voltage very low. This could be input from a sine wave generator, or a battery (doubling as representing a solar panel), or a precharged capacitor. I like to use a voltage of one microvolt, but there are other possibilities which **are always less than the voltage which is required to run the load.** This is very important!

2. There is also an exception, but this is a minor deviation involving a current division with the majority of input current (coming from a voltage source) thrown away to ground. This severely limits the input current, yet, allows for a wide variation of input voltage as you'll see down-below.

3. Capacitance and inductance are the corner stones of producing an abundance of reactive power constituting “free energy”. Impedance is your friend! (**Excessive input is your enemy.**) Since reactive power may be converted into real power using (either of) at least three unique methods of conversion, there should never be any shortage of “free energy”, aka. reactive power which is free for the taking.

These three methods (which I am aware) of converting reactive power into real power are...

1. Resistance.

2. Full rectification bridge of four diodes converting AC to DC.

3. A pair of counter-wound bifilar coils. The magnetic field of one coil will create electricity by blending with the electric field of the counter wound coil located nearby (assuming a strong coupling coefficient exists between them). And the electric field of the first coil will create additional electricity by blending with the magnetic field of the second coil.

I have two designs I'd like to share with you.

The first design is very powerful...

http://vinyasi.info/mhoslaw/Parametric%20Transformers/2021/Apr2/spark_gap_+_modifications_v5_=_schematic.BMP

It is found in the following directory on my website dated: 2021-04-28 10:22...

http://vinyasi.info/mhoslaw/Parametric%20Transformers/2021/Apr2/

The macro for its modified spark gap is found here...

http://vinyasi.info/mhoslaw/Parametric%20Transformers/2021/SparkGapMacros_Micro-Cap/FreqAmpModGroundedNeonBulbIronWrappedFilledWithAlumina.MAC

This may be what Daniel McFarland[2] invented? It's a modified gas discharge tube which does not turn ON; it does not arc at all. Yet, it manages to convert mere inductive loads into generators without the agency of moving those coils through a magnetic field such as what is described by Michael Faraday's Law of Induction. Instead, the unlit spark gap converts the inductive loads into generators of reactive power whose phases of voltage are separated from the phases of current by one-half cycle of oscillations.

The second design is less powerful. I do not know if any inventor has used this design before I stumbled upon it, recently, in my pursuit of attempting to decipher the mystery behind whatever the Ammann brothers[3] demonstrated in Denver, Colorado, in 1921 shortly before one of the two brothers was arrested for “stealing energy from the grid” which promptly put a stop to their endeavors.

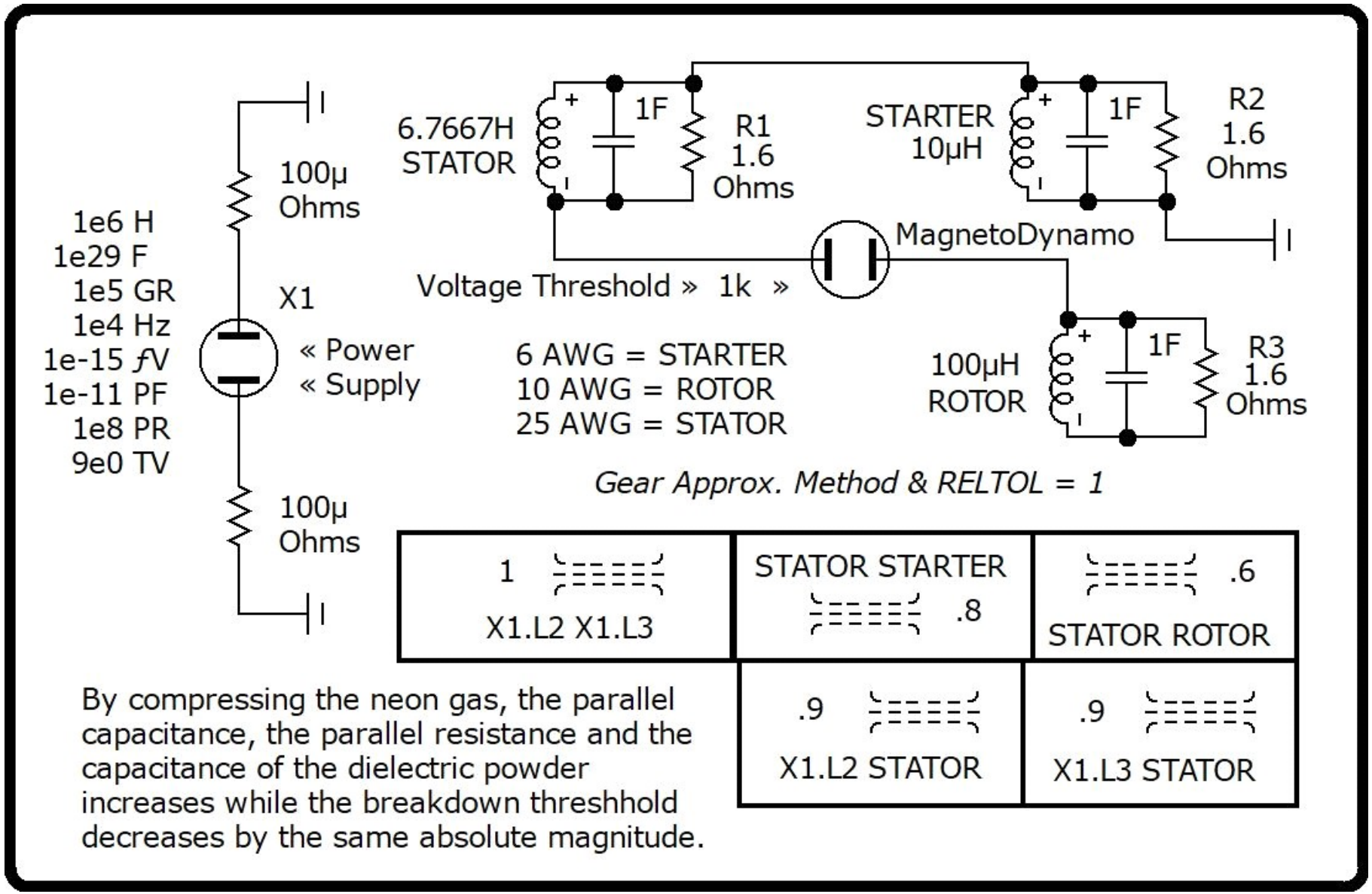
I like to craft designs garnered from my pursuit of attempting to solve historical mysterious which have become legendary in that their inventors have taken their secrets with them into their respective graves. But sometimes, on occasion, I get to stumble upon my own craftsmanship (maybe ;-).

By the way, I use a landscape format for my books, for now on, since it's easier to format my screenshots this way.

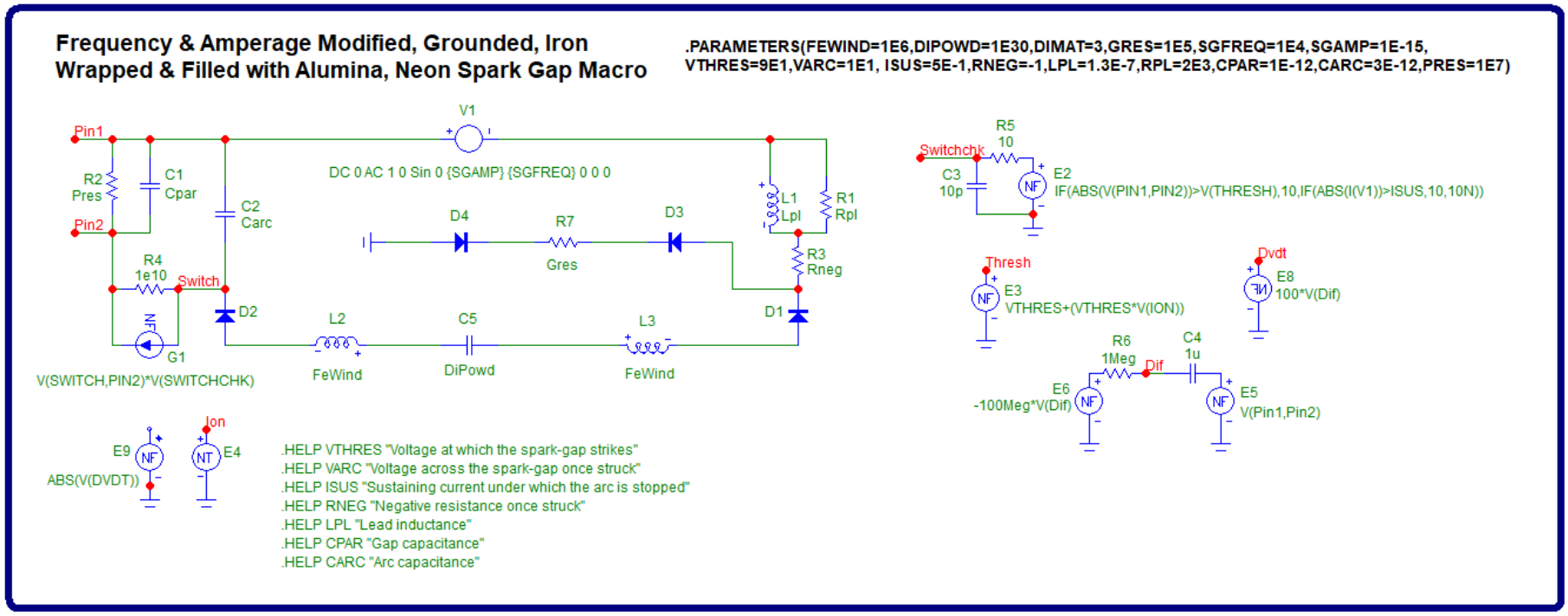
Here is the schematic of the wiring diagram of what I believe was used by Daniel McFarland's device. The fact that his device was a cross-wound pair of coils surrounding a hollow tubular bobbin - in the form of a metal pipe - is already an indication of it possibly being a modified spark gap.

Spark gaps don't need to turn ON in order to perform their magic. All that is needed is for them to be positioned nearby an inductor, or else magnetically coupled to one, such as this schematic exhibits...

2 https://duckduckgo.com/?q=daniel+mcfarland+cook&ia=web
3 https://duckduckgo.com/?q=C.+Earl+Ammann&ia=web



Here is the wiring of its modified neon bulb spark gap macro...



The inverted orientation of inductors, L2 and L3, plus their capacitor, C5, in between them suggests (to me at any rate) McFarlane's style of cross-winding surrounding his metallic, iron tube upon which he wrapped his coils. An ionizing gas was filled inside of his tubes. One end of his cross-winding connected both bifilar windings (L2 with L3). The other end of both coils was terminated with a capacitor (represented, here, by: C5). The grounded condition of diodes, D4 and D3, indicate to me that the interior of his metallic tube was electroplated with aluminum and the inner surface of this plating was conditioned with an electrolyte of either borax or baking soda while an alternating current was passed into, and out of, his electrolyte through the plating and its surrounding tube. This conditioning placed a thin layer of aluminum oxide (known as: alumina) onto the inner surface of the electroplated aluminum, thus, causing the plating to act as a diode.[4] Since the entire surface of the electroplating was a parallel arrangement of diodes pointing their anodes inward towards the center of the metallic tube (once the electrolyte was drained out of it after the process of conditioning his tube has been completed), and the ionized gas has a certain resistance - represented, here, by resistor: R7, and this “ground” is connected to the macro at one terminal of resistor: R3 (whose negative resistance represents the ionizing feature of the gas which is held inside of the tube), then (consequently) this almost completes my modifications of a simple spark gap.

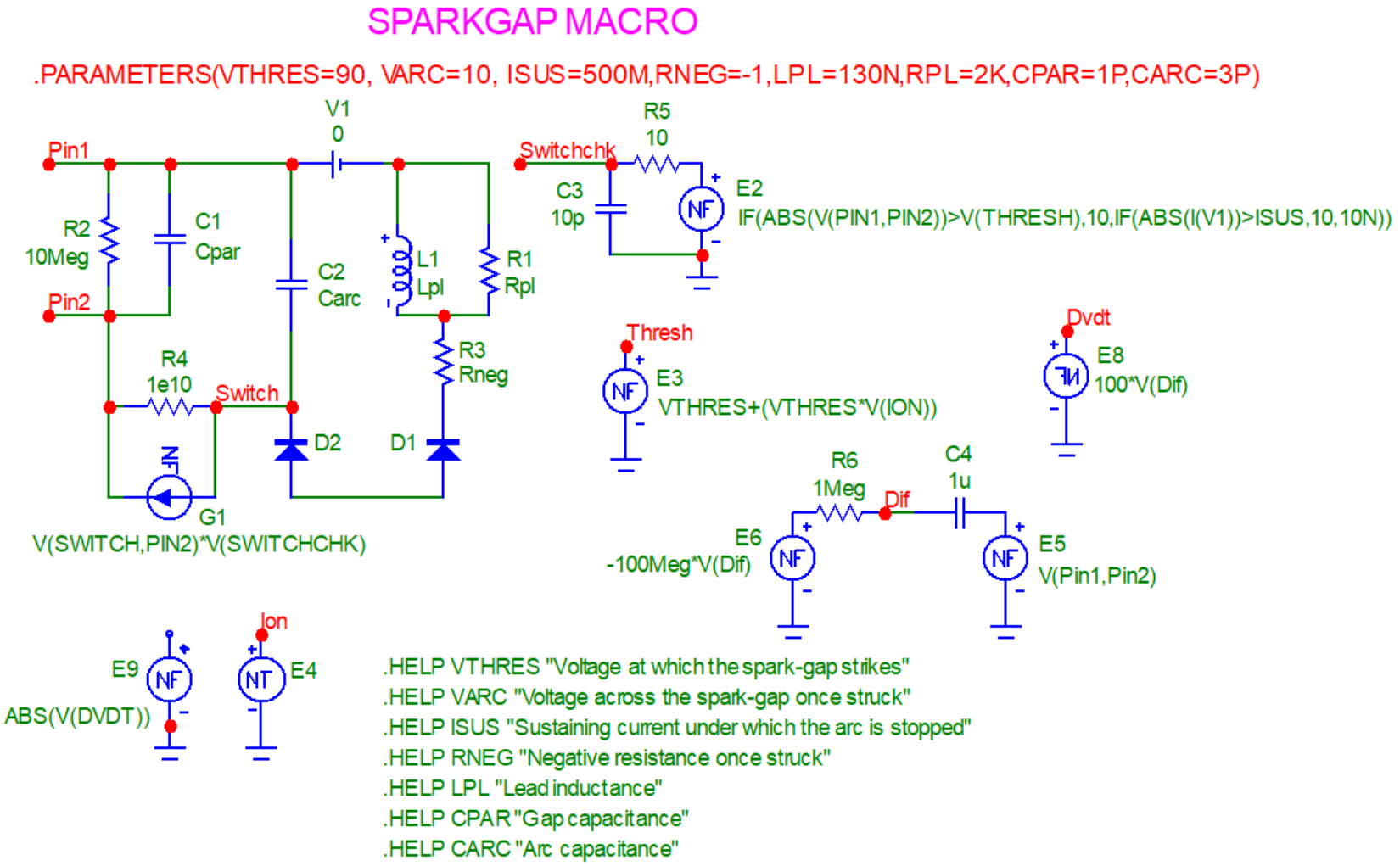
Spark gaps possess a transistor element, represented here by the two diodes, D2 and D1. Their input goes nowhere (shown, below). But I take advantage of this potentiality by wrapping two coils, L2 and L3, around this gas discharge tube and positioning them (in this simulation) where they are supposed to be: in between these two diodes.

4 http://www.sparkbangbuzz.com/els/borax-el.htm

Adding an electroplating to the interior of this metallic gas discharge tube adds an additional transistor which is represented by diodes: D4 and D3. The resistance of the ionized gas, represented by resistor: R7, serves as the true “ground” in conjunction with the presence of the simulated ground to the left of these two diodes.

I replaced the zero voltage battery, shown below, with a sine wave generator (shown above) which inputs a default frequency of 10k Hertz (SGFREQ) riding on an amplitude of voltage (SGAMP) which is one femto volt (1e-15V).

Here is the original, non-modified spark gap macro...

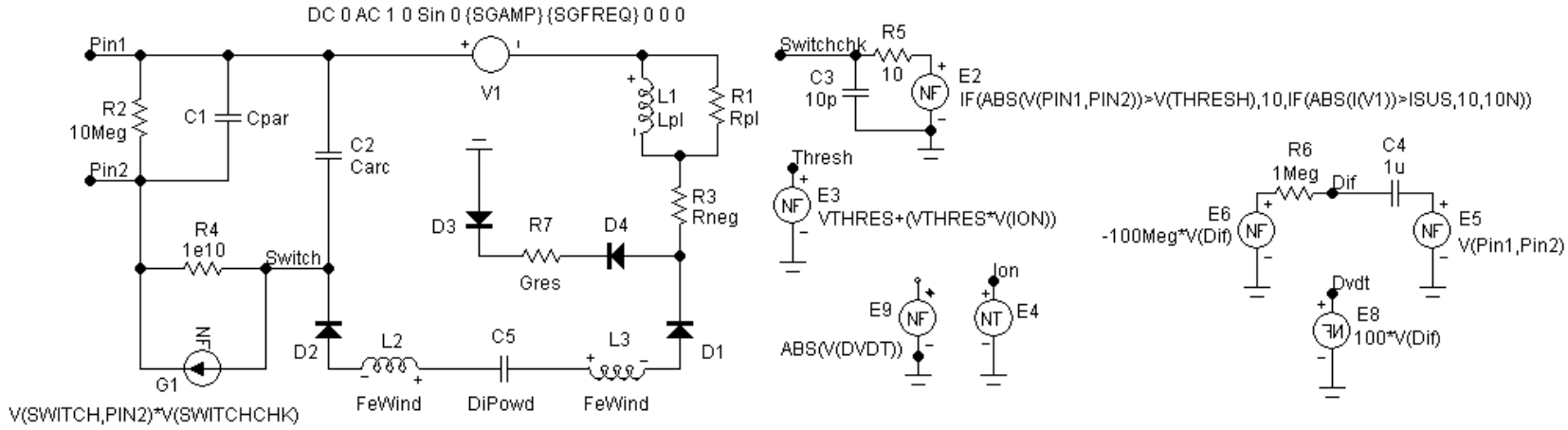


At the time when I crafted these modifications, I did not know what I now suspect that the so-called “ground” which I had inserted just below resistor, R3, is actually an electroplating on the inner surface of this customized gas discharge tube. Now, I know better.

Here is the original modified spark gap with all of the explanatory text which I left out of the macro up-above (only because I am too lazy to transfer it ;-)...

GROUNDED & BENT IN THE MIDDLE, NEON-FILLED, COPPER TUBING, FREQUENCY & AMPLITUDE MODULATED, SURROUNDED BY AN IRON WINDING REPRESENTS A PAIR OF INVERTED COILS » L2 & L3, & FILLED WITH POWDERED TANTALUM OR ALUMINA IS CAPACITOR » C5.

.PARAMETERS(FEWIND=1e6,DIPOWD=1e30,DIMAT=3,GRES=1e5,SGFREQ=1e4,SGAMP=1e-15,VTHRES=9e1, VARC=1e1, ISUS=5e-1,RNEG=-1,LPL=1.3e-7,RPL=2e3,CPAR=1e-12,CARC=3e-12)

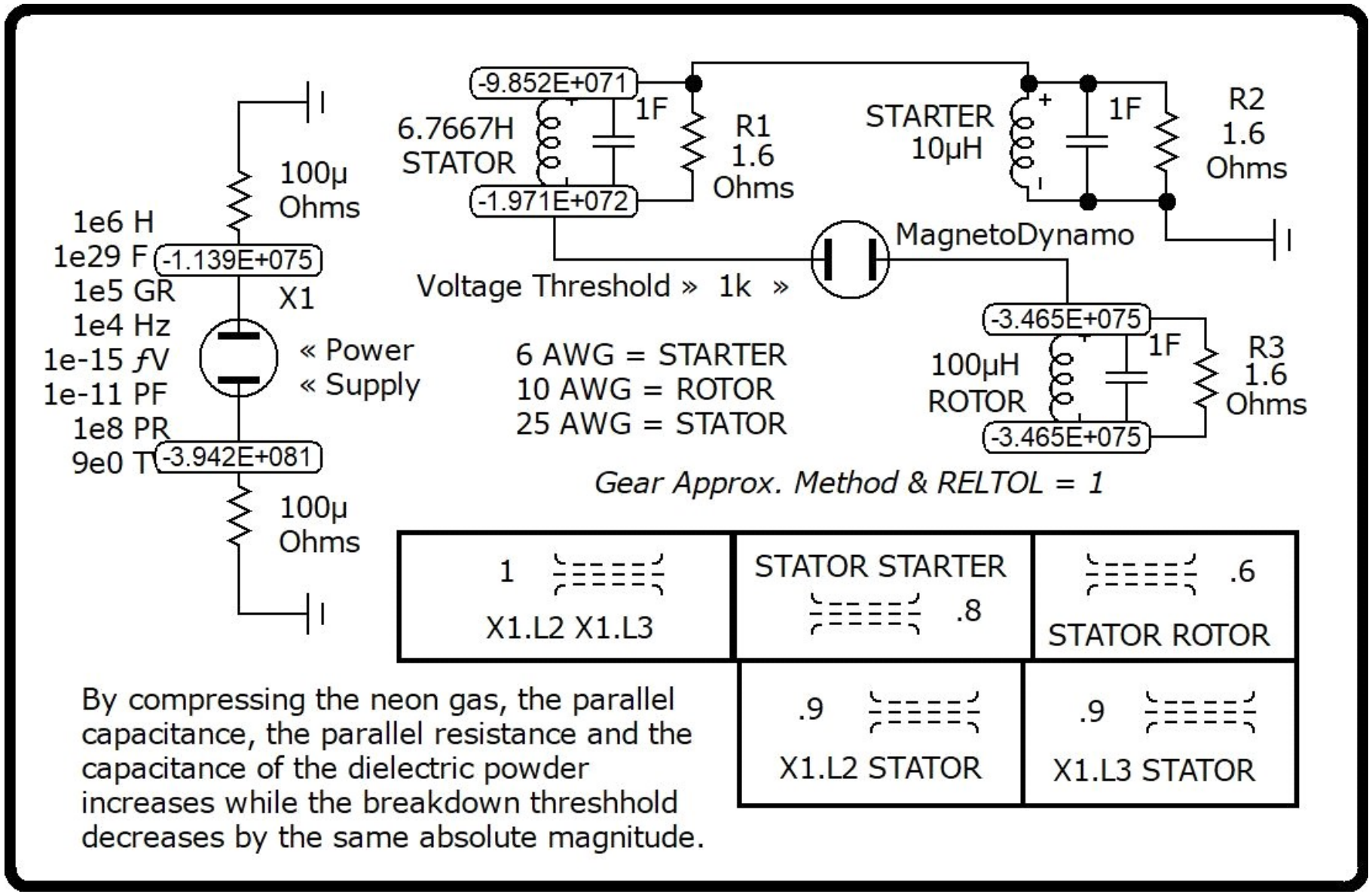


.HELP FEWIND "Inductance of L2 and L3, of inverted windings and undefined series resistance, is an iron coil surrounding a bent-in-the-middle copper tube filled with neon gas."
.HELP DIPOWD "Capacitance of C5 suffuses the interior of this neon bulb, spark gap." .HELP GRES "Resistance of ground connection"
.HELP DIMAT "Equivalent series resistance of the dielectric material within C5 defaults to 3 Ohms (analogous to tantalum or alumina dielectric)."

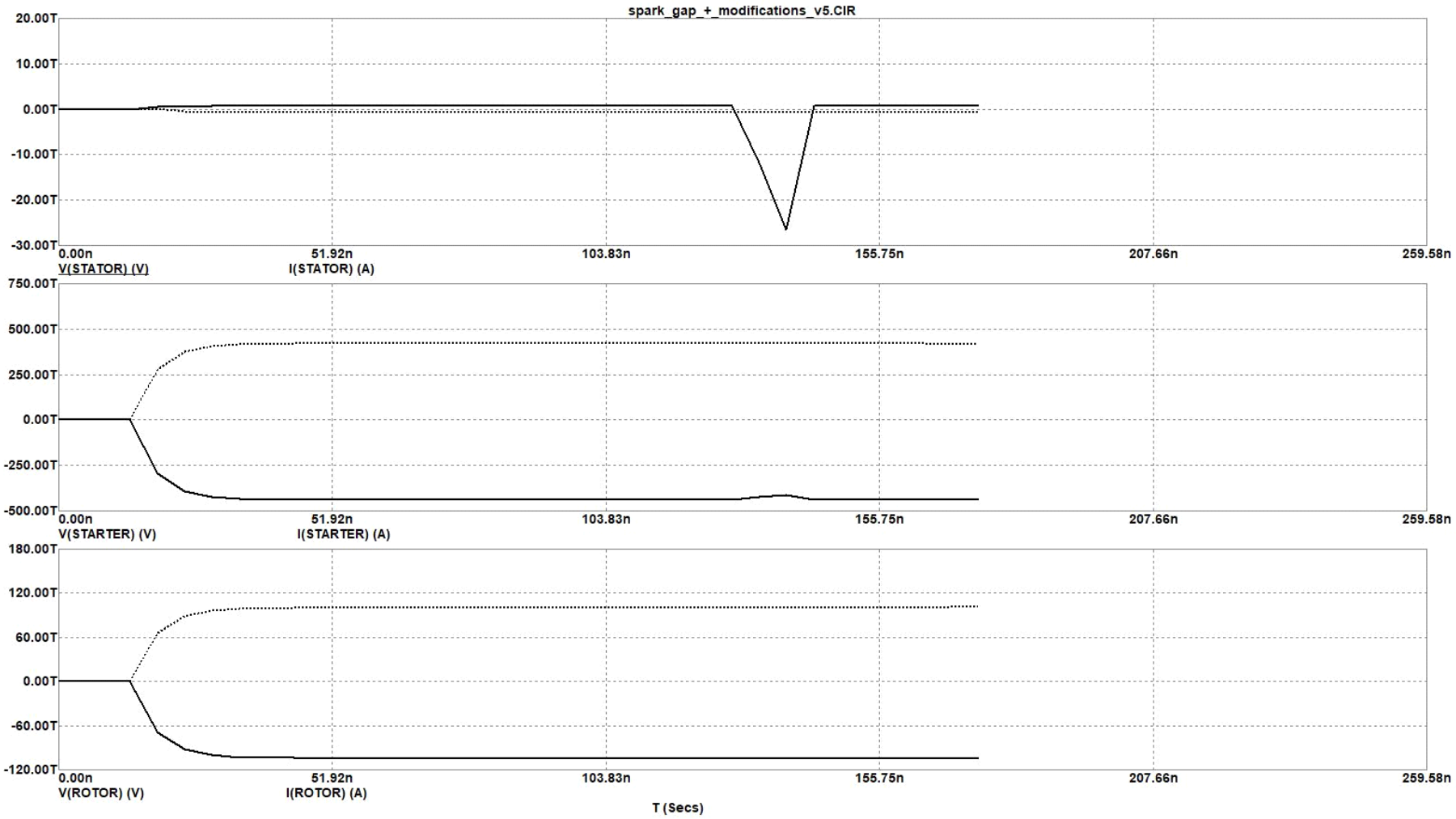
16 micrometers of neon gas and powdered iron and powdered tantalum or alumina (aluminum oxide) between two electrodes is Nikola Tesla's TriMetal Generator. It is assumed that X1.L2 and X1.L3, within this macro, will be magnetically coupled to another inductor, outside this macro, from within a circuit which uses this spark gap. This prevents suppression of over-reactance by electrically isolating the spark gap from the load.

.HELP SGFREQ "Frequency of sine wave input into spark gap, neon bulb"
.HELP SGAMP "Amplitude of sine wave input into spark gap, neon bulb"
.HELP VTHRES "Voltage at which the spark-gap strikes"
.HELP VARC "Voltage across the spark-gap once struck"
.HELP ISUS "Sustaining current under which the arc is stopped"
.HELP RNEG "Negative resistance once struck"
.HELP LPL "Lead/electrode inductance"
.HELP RPL "Lead/electrode resistance"
.HELP CPAR "Gap capacitance"
.HELP CARC "Arc capacitance"

Here are the nodal voltages of this circuit after less than 200 nanoseconds of simulator runtime...



Here is its output...



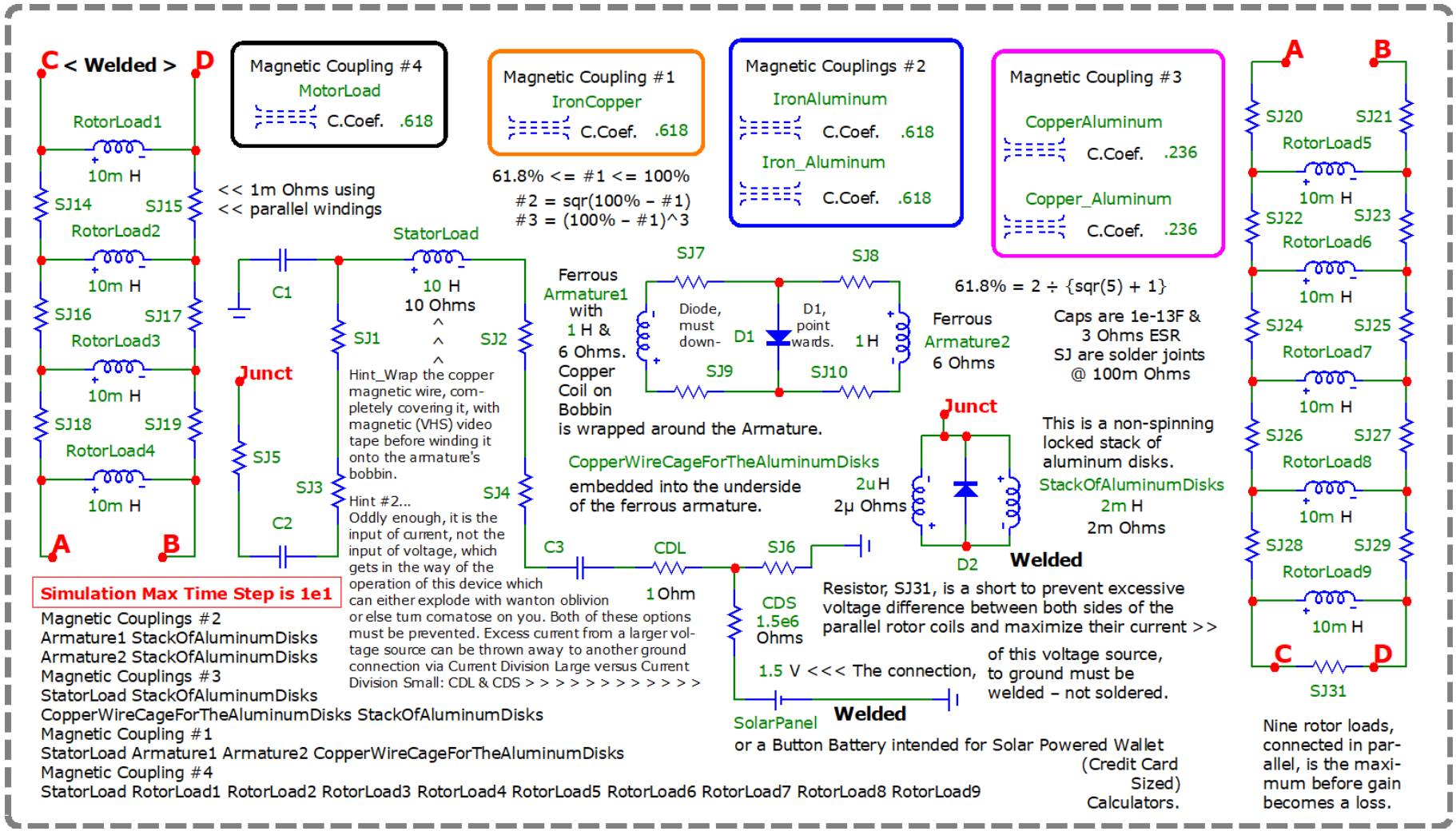
The next screenshot is of the second circuit which I wish to share with you...

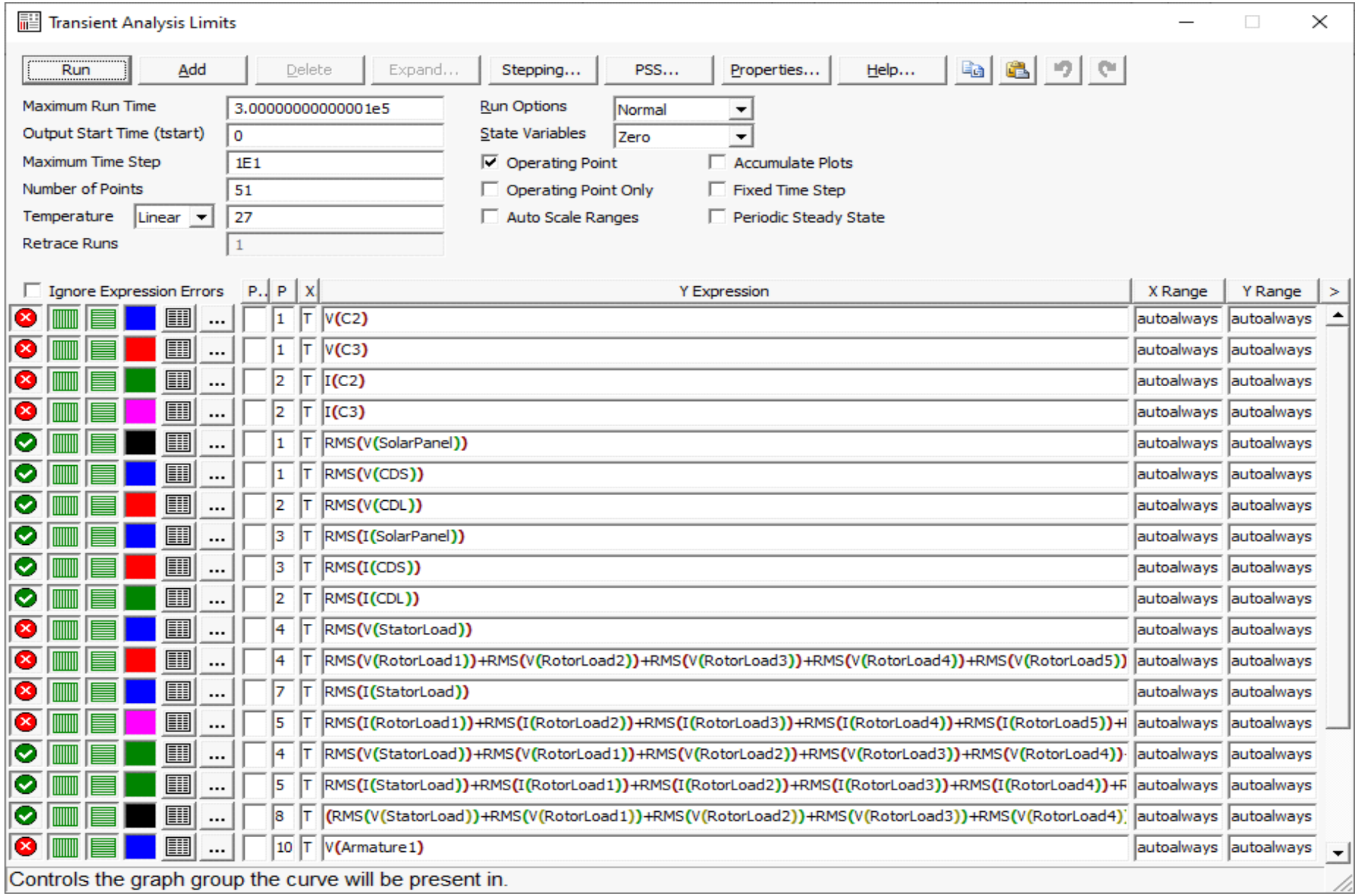
http://vinyasi.info/patent/pri-vate/load/now7a3,%20halved%20voltage,%20same%20current%20as%20now7a2,%20schematic.png

It's found in this directory...

http://vinyasi.info/patent/pri-vate/load/

The previous circuit was simulated with a GEAR approximation method and a relative tolerance, RELTOL, of 1. Yet, the following circuit works just as well with a TRAPEZOIDAL approximation method and a RELTOL of the simulator's default setting of 1m (under Options / Global Settings). I practically adore this circuit for its utter simplicity if you can ignore all of the embedded text!...





Yet, it manages to produce what I like to call “staccato wedgies”. These wedgies are the analog of a self-damping wave...

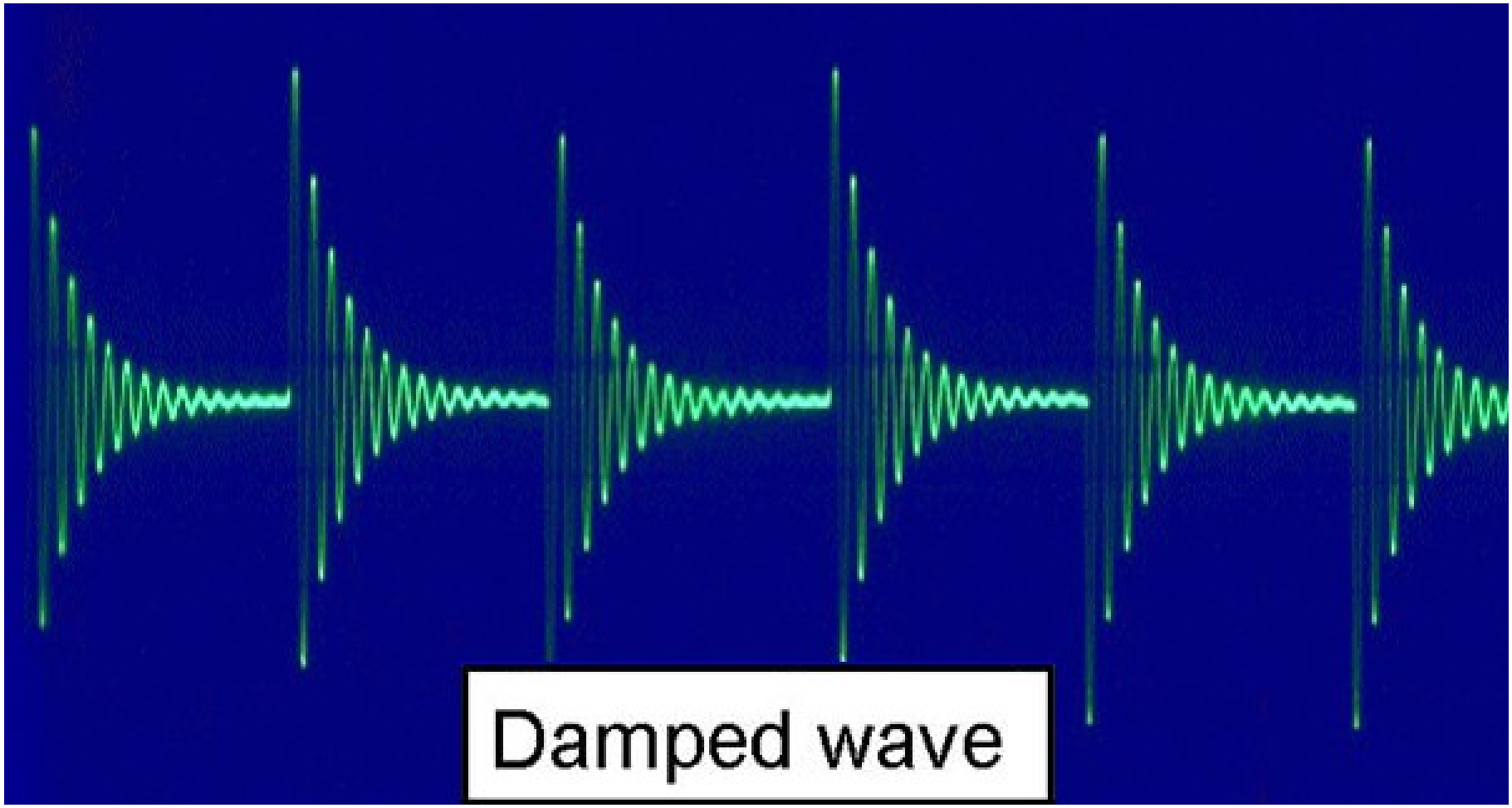
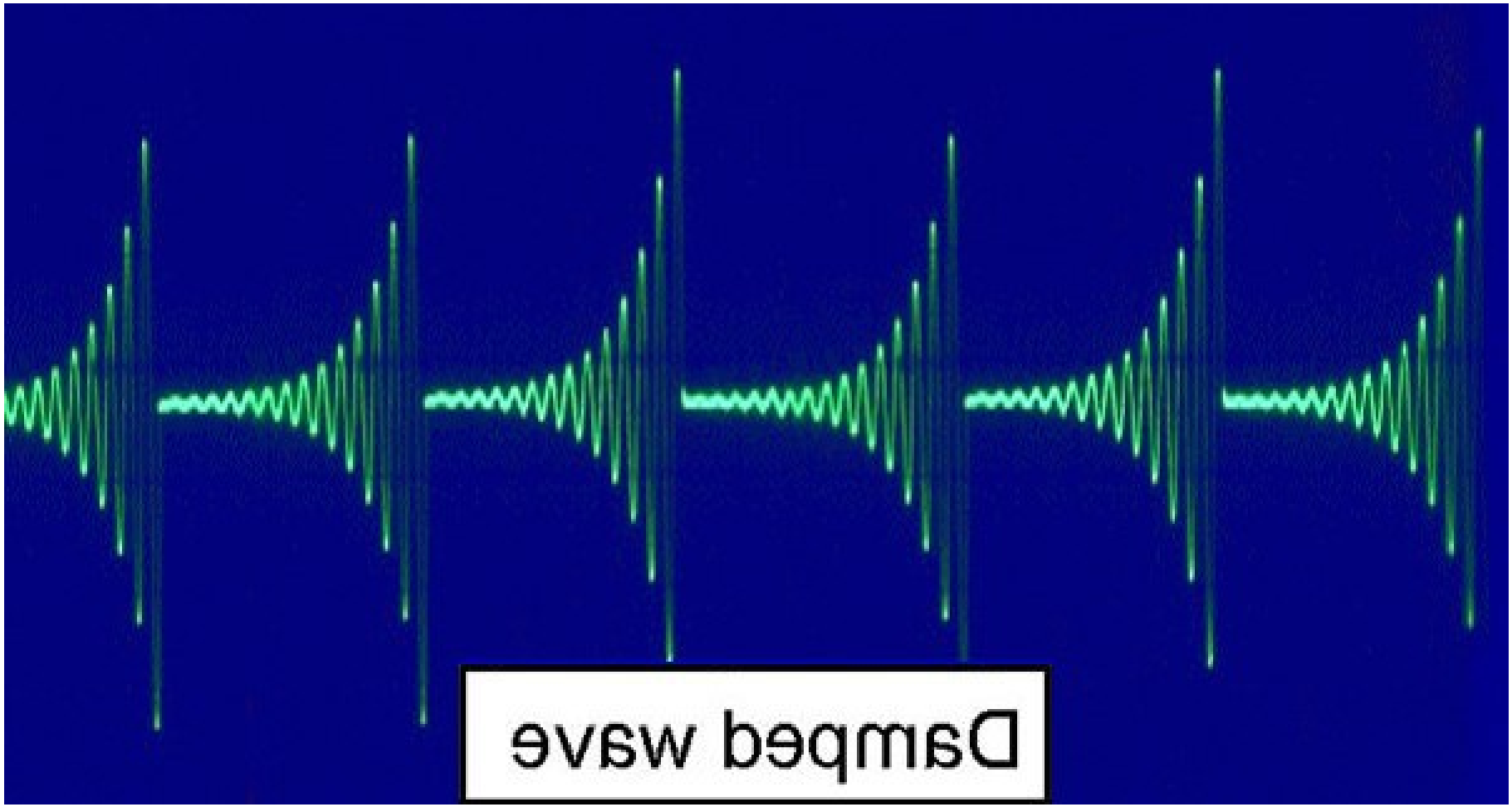


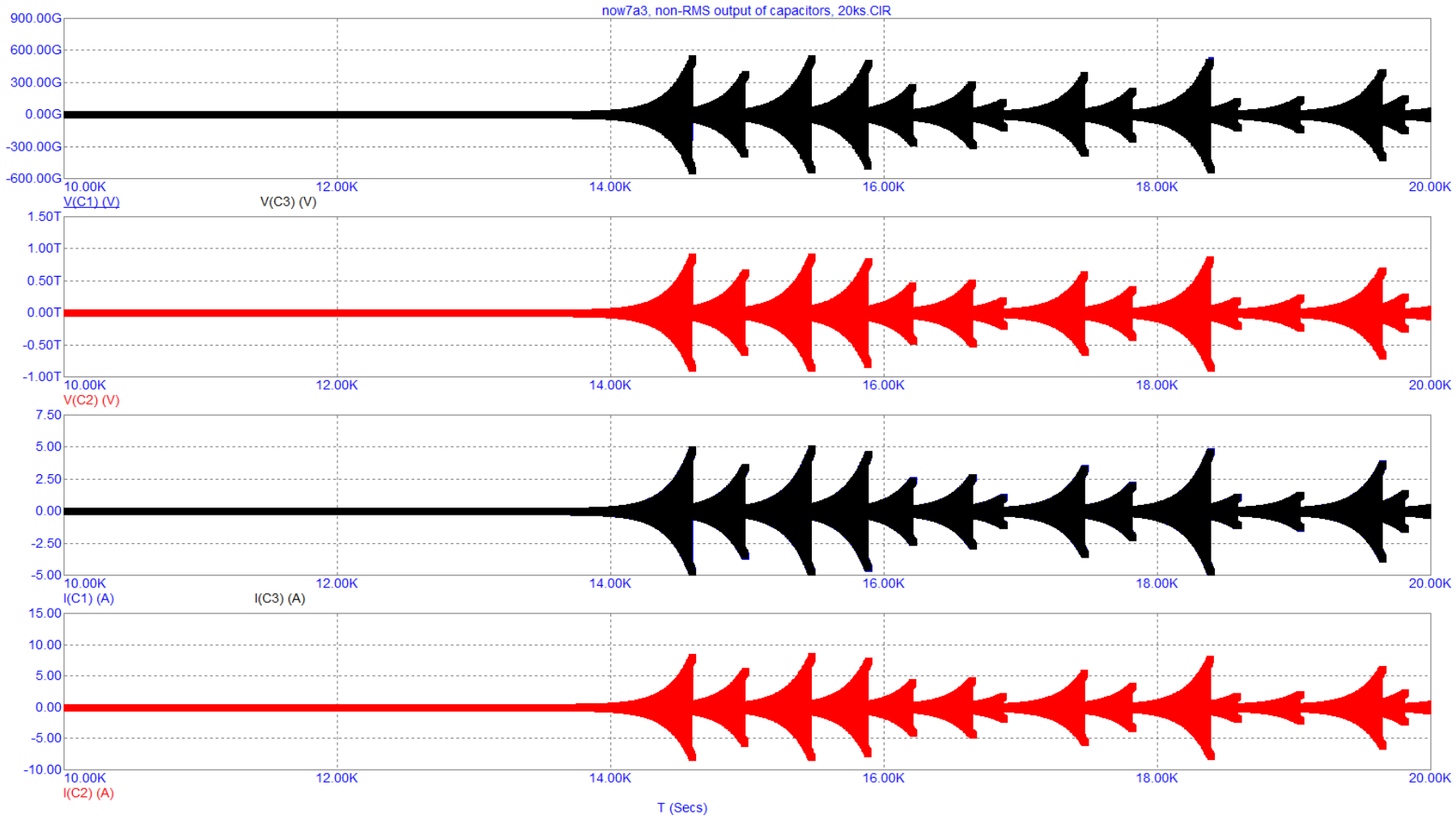
Photo courtesy of The Royal Rife Story...

http://theroyalrifestory.com/chapter%20_19_dr_rifes_gating.html

...with the difference that they possess a reversal of their direction in time...



Instead of diminishing, they escalate with the additional advantage of periodically collapsing to prevent the destruction of their host-circuit...

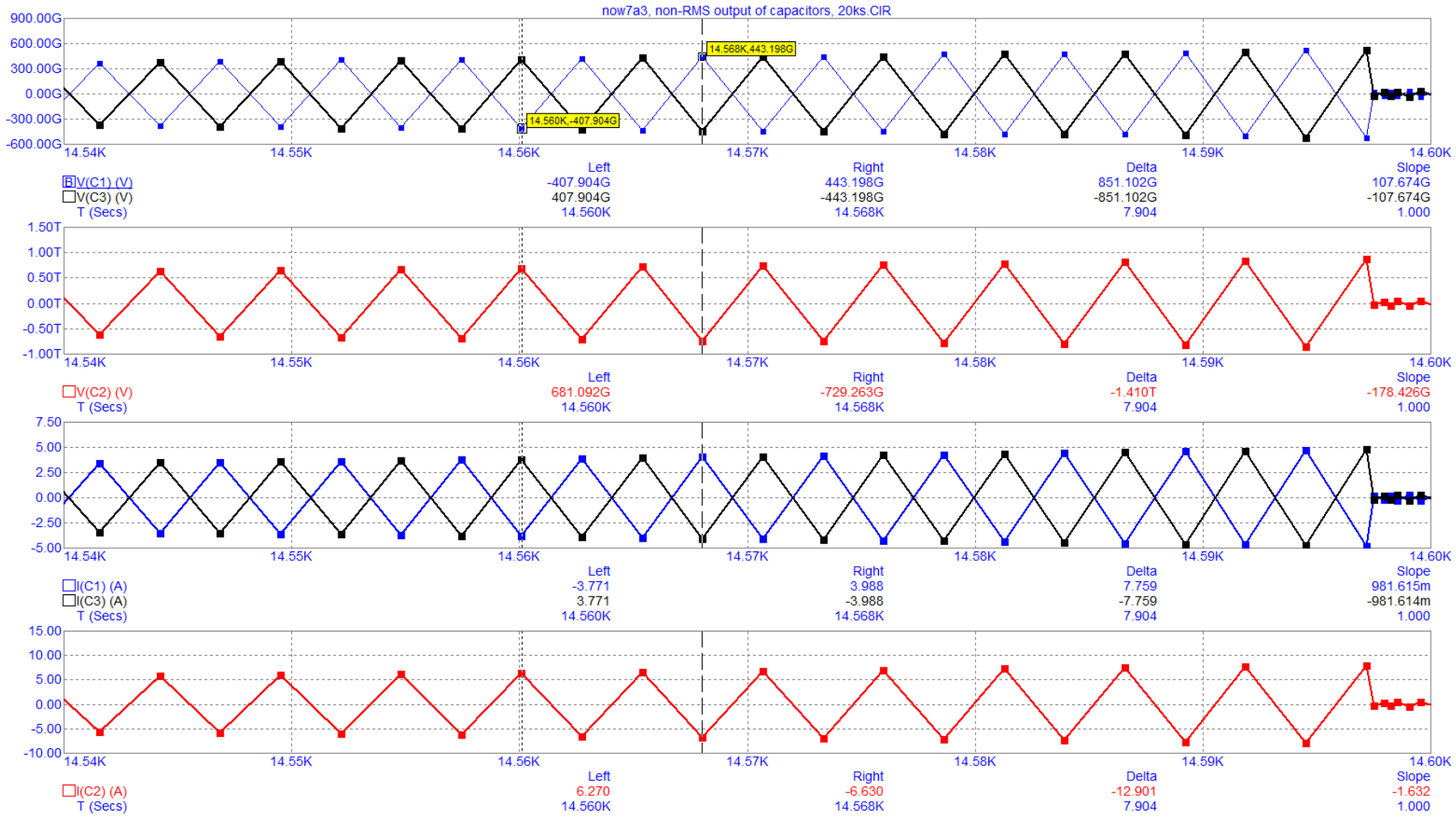


Here is a closeup view of the capacitors (shown above) exhibiting a triangular waveform which indicates a condition of the non-saturation of current.

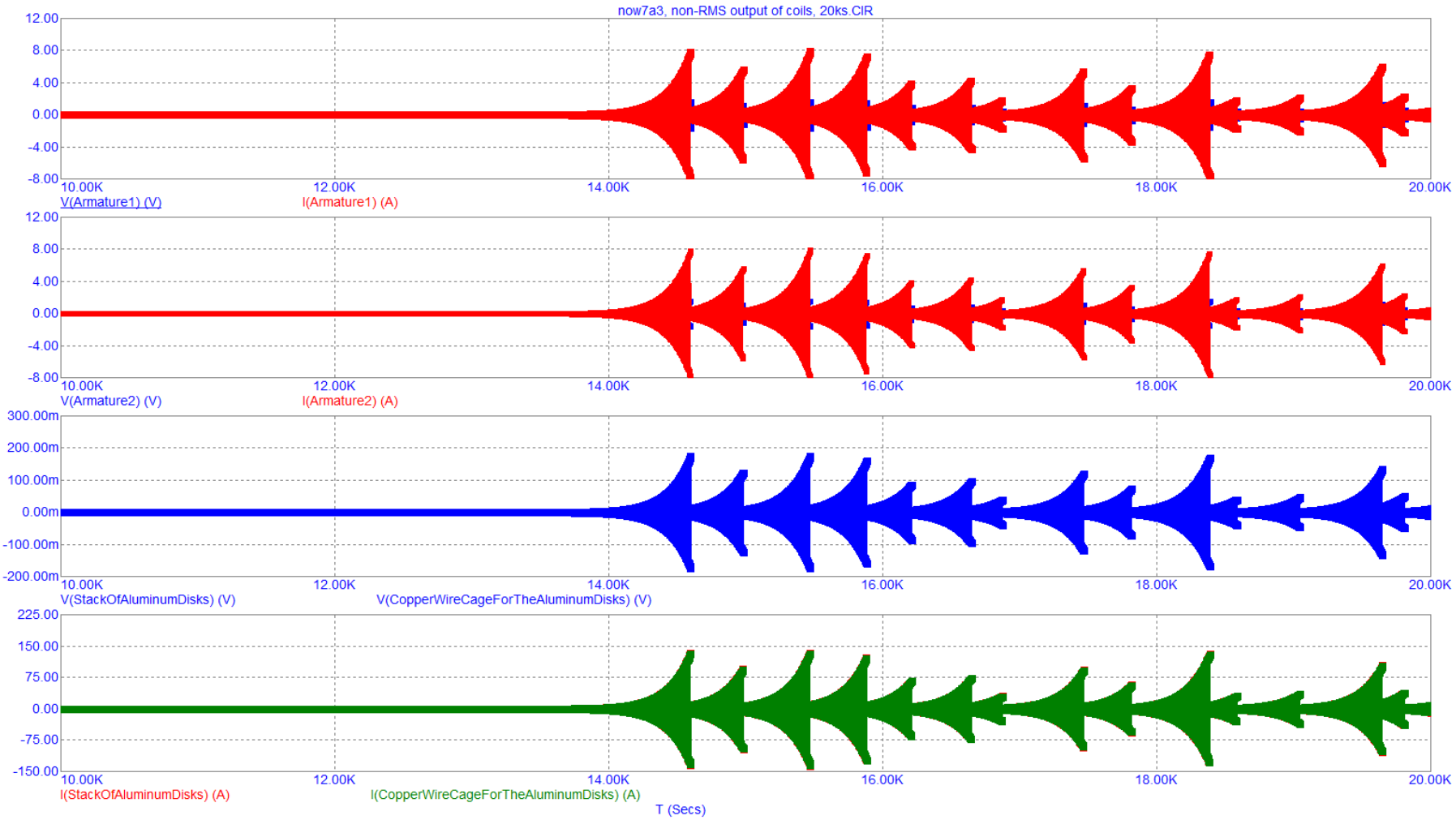
Saturation of current will result in a nice sine wave plus back EMF and a time-displacement of a 90° lagging current (behind voltage). Conversely, the non-saturation of current will result in triangular waves, no back EMF(!) and a complete inversion of phases (between voltage and current).[5]

5 https://www.monolithicpower.com/en/how-to-avoid-inductor-saturation-in-your-power-supply-design

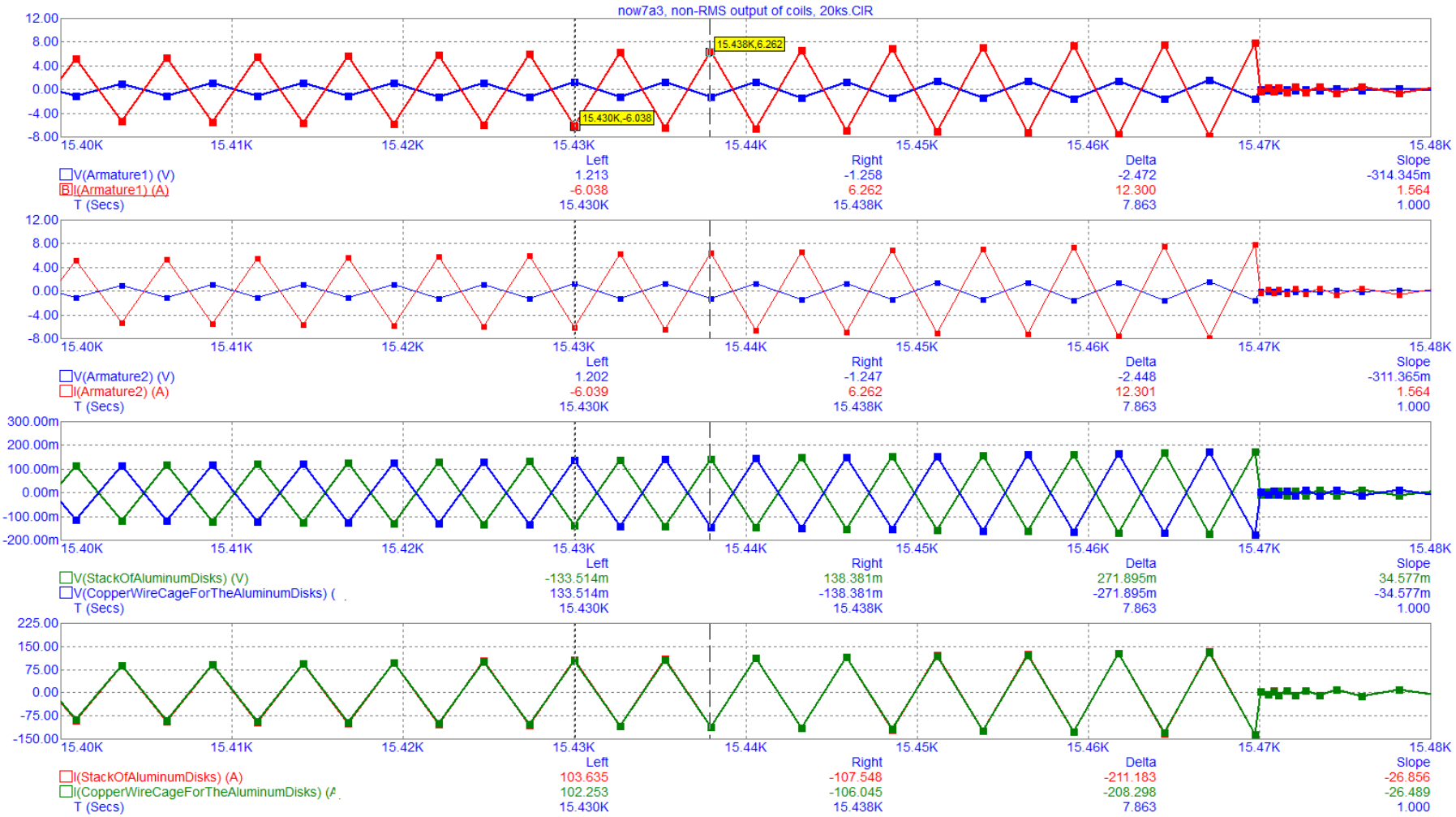
All of these capacitors are consuming power due to their phases of voltage and the phases of their current are in complete alignment with each other with zero angular (temporal) difference between them...



Notice the very consistent eight second wavelength, up-above? Yet, the pulses of each surge, followed by its collapse, are a bit irregular in both their amplitude and their frequency...

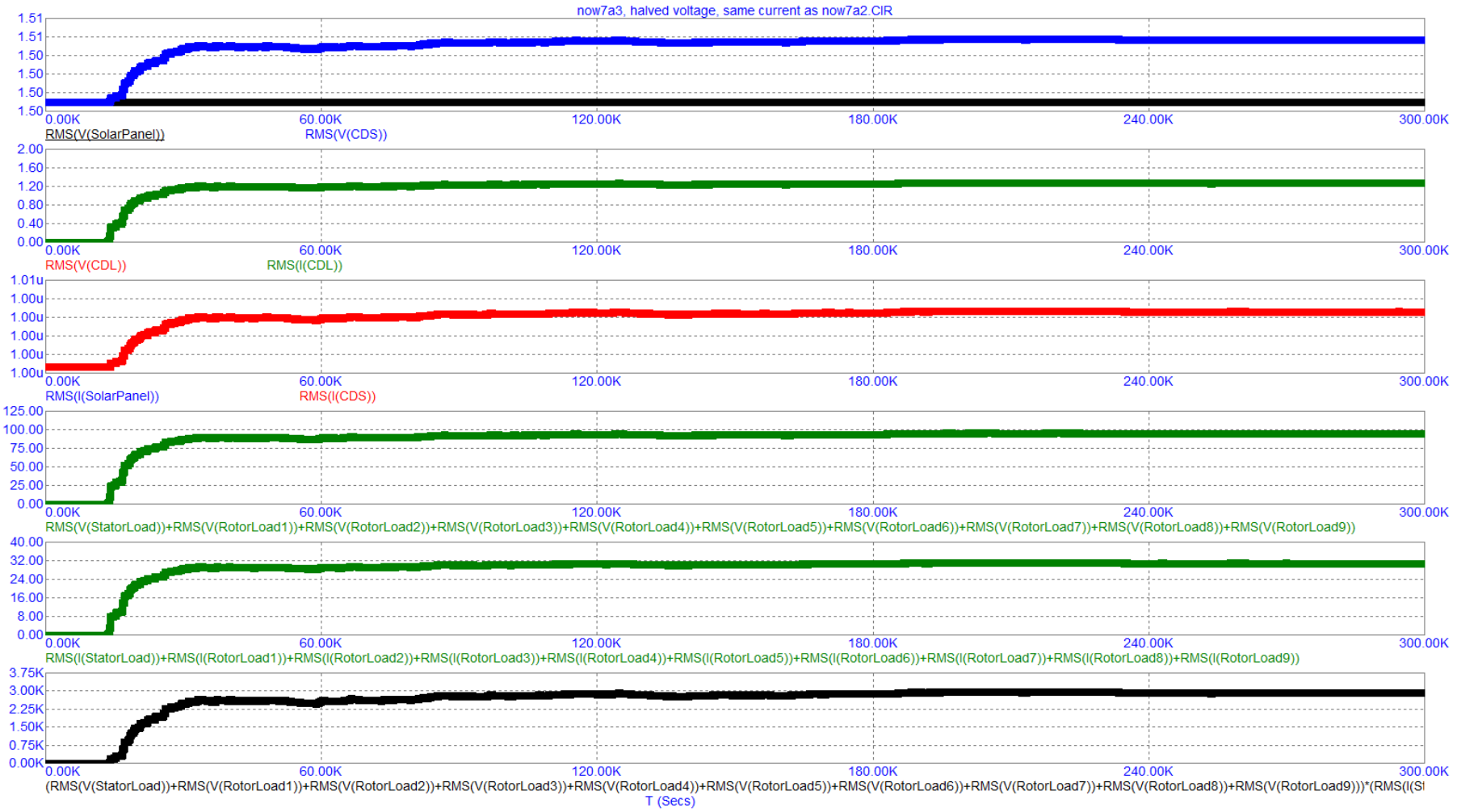


Here is the closeup view of the output of the coils (which are displayed up-above)...



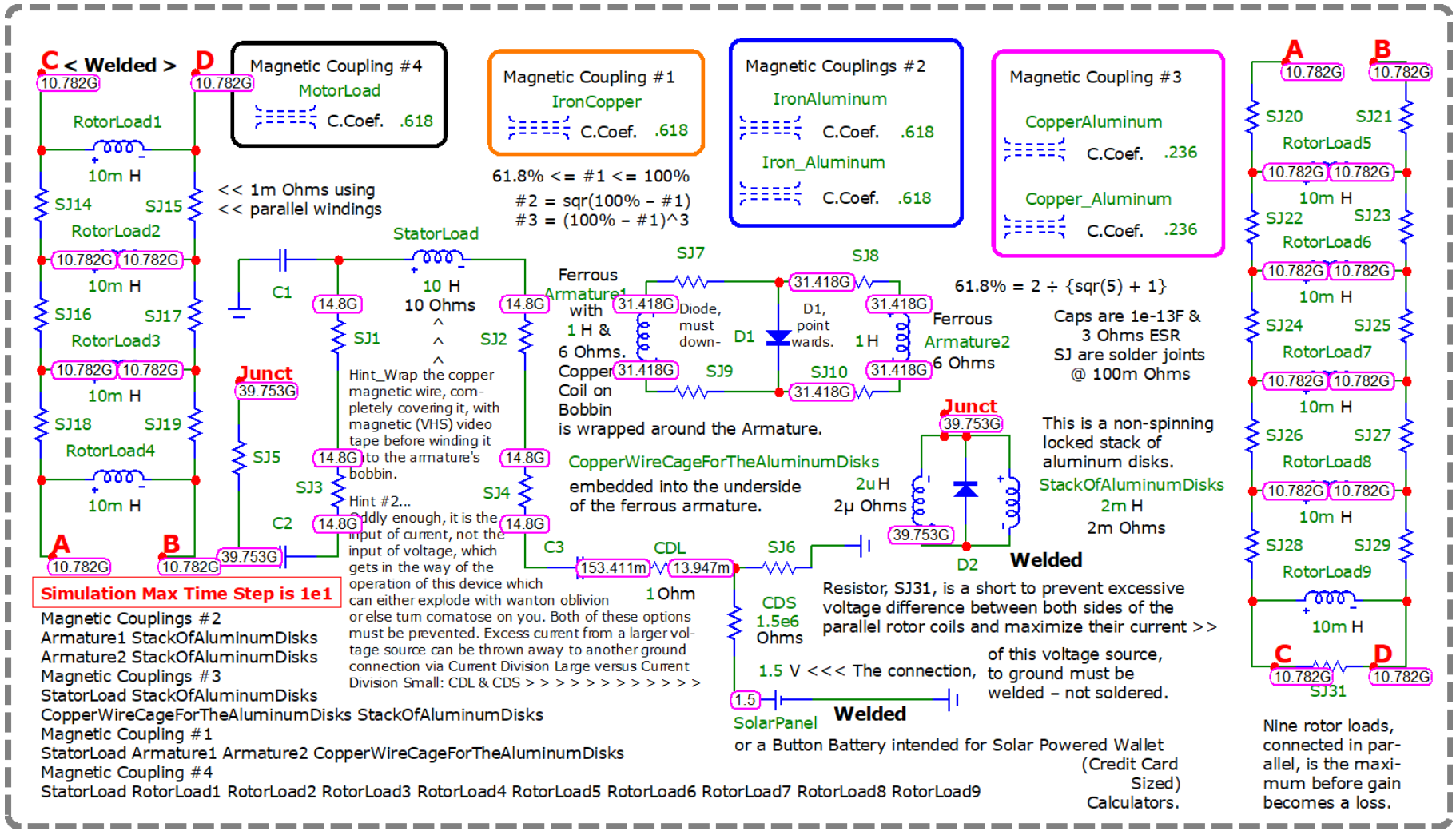
Notice how the voltage phase of electricity has been separated from the current phase within the Armature Coils #1 and #2 and within the Stack of Aluminum Discs? This is essential for the generation of reactive power (VARS), and overunity, to occur to makeup for the consumption of real power (watts) within the capacitors and surpass their consumption of power in order to accumulate an excess of reactive power given enough time. This factor of “time” can vary as much as tens of thousands of seconds versus mere nanoseconds or anything else in between depending upon the efficiency of the design of the overunity circuit.

This circuit archetype makes it very easy to maintain a stable RMS output...



By the way, don't let the elevated nodal voltages scare ya. Maybe, it might help to immerse the bare nodes (junctions) of this circuit in a dielectric block?...[6]

6 http://vinyasi.info/graham/max%20acceleration%20for%20a%202002%20RAV4EV/Di-Electric%20Cage/



I suspect that this circuit is a variation upon the theme of a Kromrey[7] generator[8] (also known as a Kromrey converter) and a reincarnation of Tesla's Special Generator[9] (mentioned by William Lyne[10] in his book, entitled: "Pentagon Aliens" (available for purchase[11] on Amazon), and is also

7 https://web.archive.org/web/20220319101647/http://www.cheniere.org/books/CombinedKromreyReports.pdf
8 https://duckduckgo.com/?q=kromrey+converter&ia=web
9 https://www.bibliotecapleyades.net/ciencia/pentagonaliens/pentagonaliens08.htm
10 http://teslasidealflyingmachine.com/
11 https://www.amazon.com/gp/product/0963746774

mentioned in Thomas Commerford Martin's book on the writings and inventions of Tesla (available at Amazon [12] and downloadable[13] from archive.org). I think that it is the large pair of armatures of one Henry, each, at: Armature1 and Armature2, which hints at these similarities among these various circuits (by other inventors) along with the two diodes in each circular loop: at the pair of armatures and inside of the "Copper Wire Cage for the Aluminum Disks" (which is paired with the "Stack of Aluminum Disks").

To quote Lyne quoting Tesla: "for every two hundred pounds of iron added to Tesla's Special Generator, one horsepower is increased at its output". *{footnote #6, above}* This is predicated upon the principle of magnetic remanence,[14] not magnetic flux,[15] popular in computer core memory[16] dating from the years of 1955 until 1975. And also found evident within the Perpetual Motion Holder experiments made popular (but not invented) by Edward Leedskalnin[17] (who also built Coral Castle[18] outside of Miami, Florida).

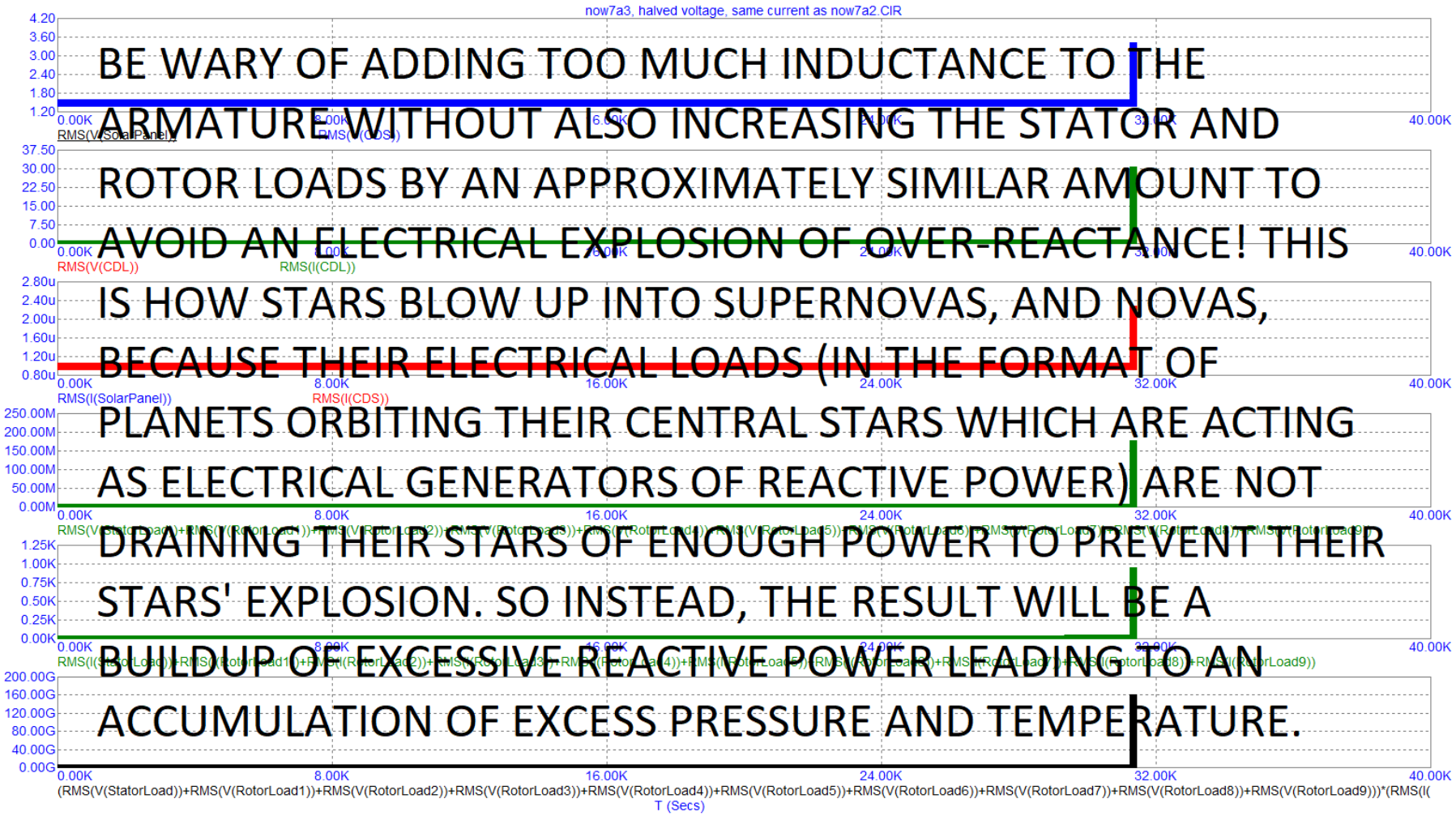
This property of magnetic remanence is similar to a flywheel in that an impression of inertia is left behind in the ferromagnetizable substance that is not at all related to the momentum which put it there. This is where the mechanical analogy breaks down. Instead, this property of magnetic remanence is related to the size of the coils wrapped around all of, or a portion of, this ferromagnetizable mass along with the size of this mass. This is where the increase of power is going to be gained from. Not from the input of magnetic flux entering into this massive storehouse of magnetic memory, but from the mass, itself, along with the size of the winding which puts it there.

This would suggest how to build this circuit is by not attempting to put all of the inductance into the iron core of its "Armature", but to magnetically couple an extra mass of ferromagnetizable substance held outside of this "core" material whose properties, and substance, should probably be exactly the same composition as the core material?

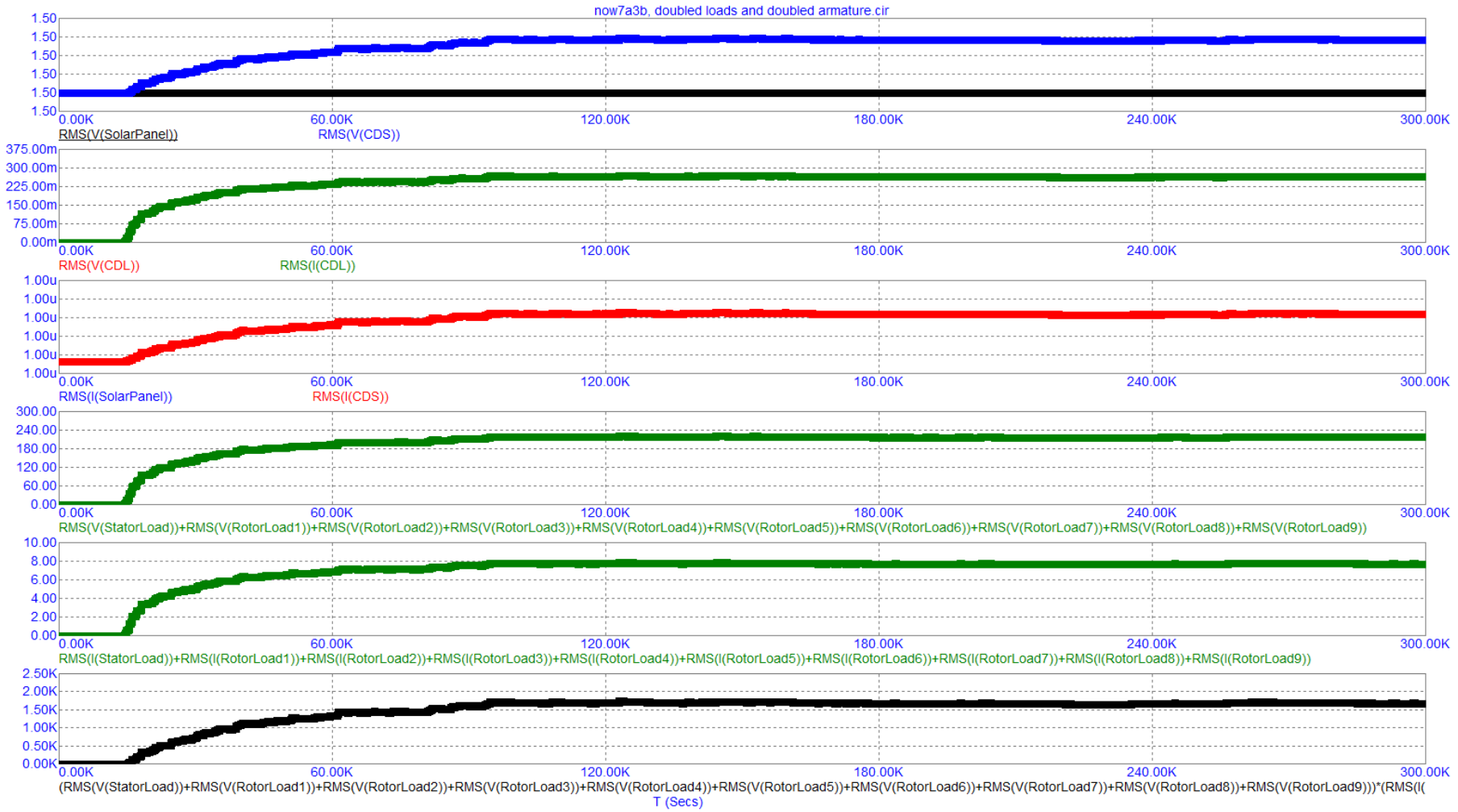
I don't know... It's just a hunch. I could be wrong; or, right, as the case may be... ;-)

Look what happens when these two inductances (representing the singular toroidal armature), Armature1 and Armature2, are increased by a factor of ten (from a value of one Henry to a value of ten Henrys) without a corresponding increase made to the loads represented by the StatorLoad and the nine RotorLoads(1-9) resulting in their output explodes...!

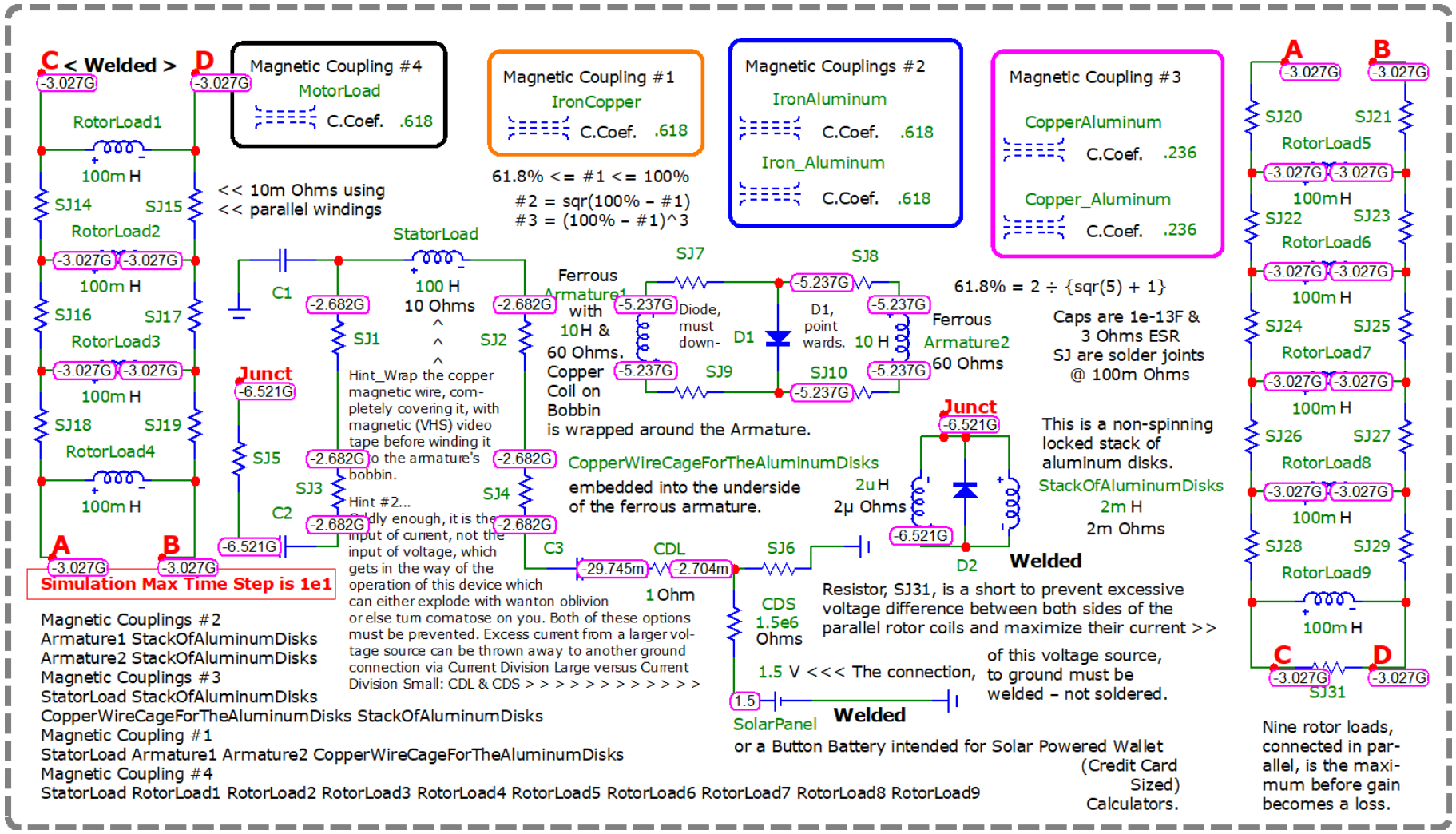
12 https://read.amazon.com/kp/embed?asin=B08LZLCQ89&preview=newtab&linkCode=kpe&ref_=cm_sw_r_kb_dp_2RK589XR163430E026DE
13 https://duckduckgo.com/?q=site%3Aarchive.org+Thomas+Commerford+Martin+the+inventions+and+writings+of+nikola+tesla&ia=web
14 https://duckduckgo.com/?q=magnetic+remanence&ia=web
15 https://duckduckgo.com/?q=magnetic+flux&ia=web
16 https://duckduckgo.com/?q=magnetic+core+memory+computer&ia=web
17 https://duckduckgo.com/?q=edward+leedskalnin+perpetual+motion+holder&ia=web
18 https://duckduckgo.com/?q=edward+leedskalnin+coral+castle&ia=web



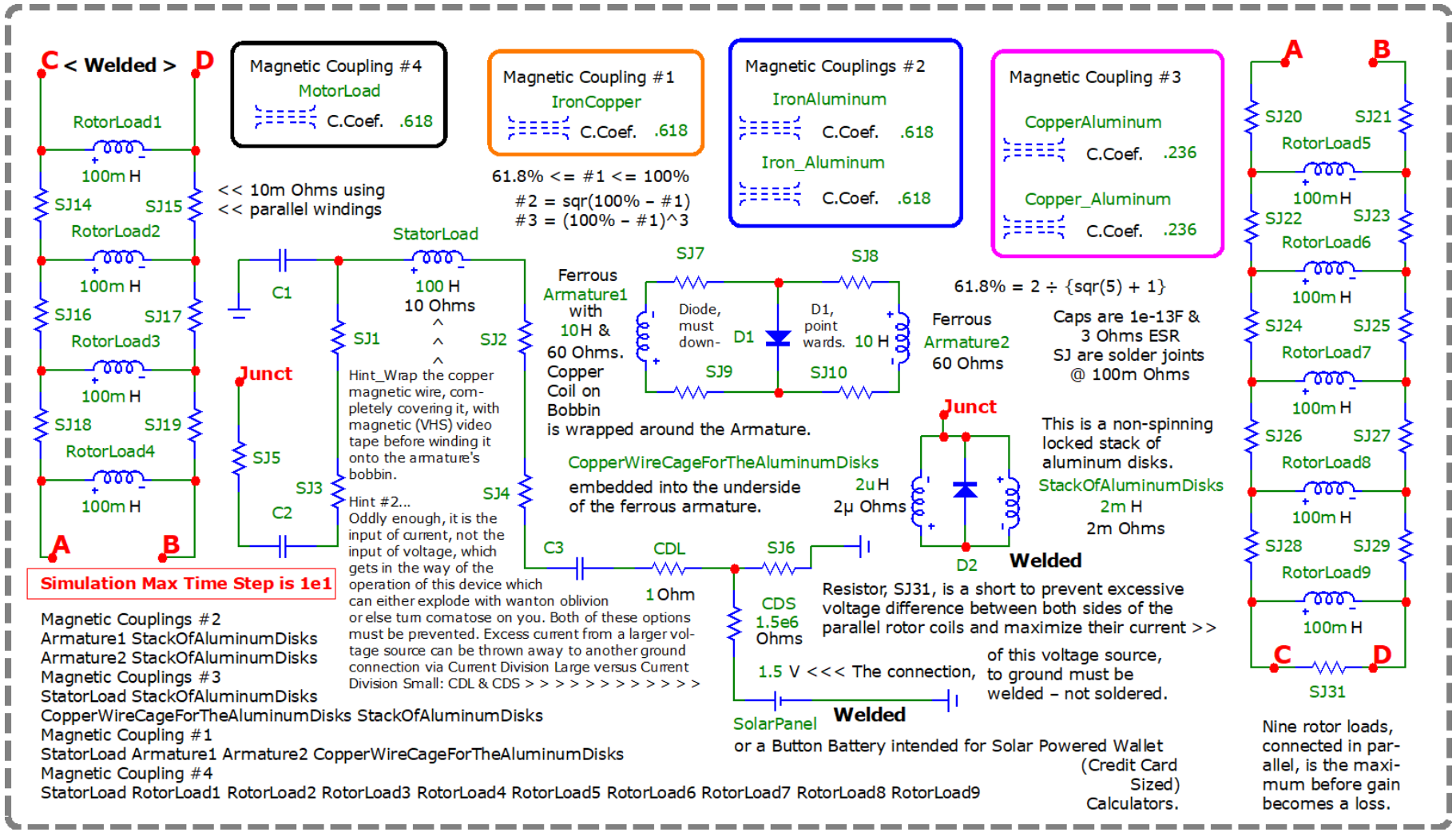
But look what happens when I also increase the Stator and Rotor loads by a similar factor of ten: everything is fine...



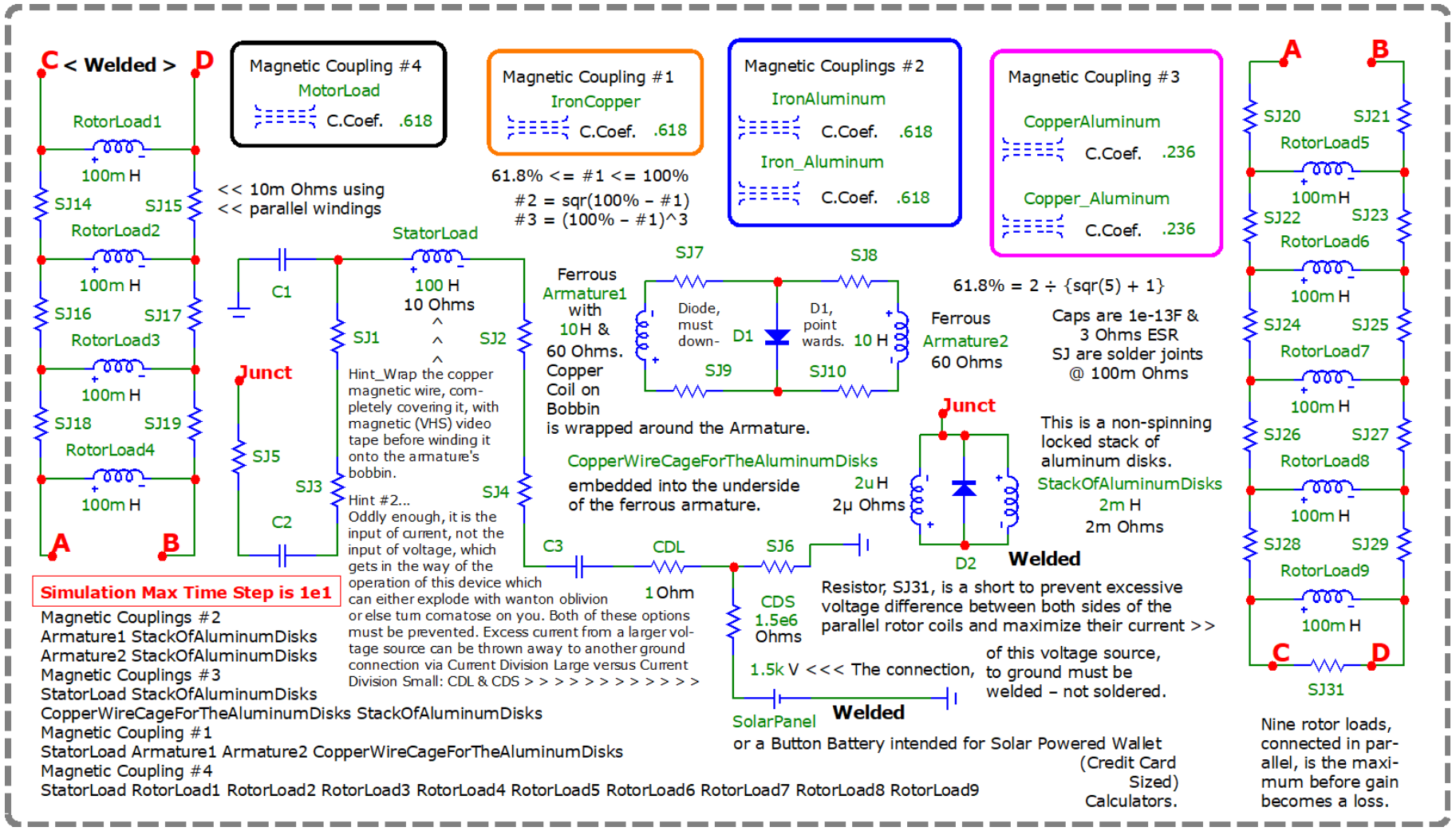
Nodal voltages after 300k seconds of runtime...

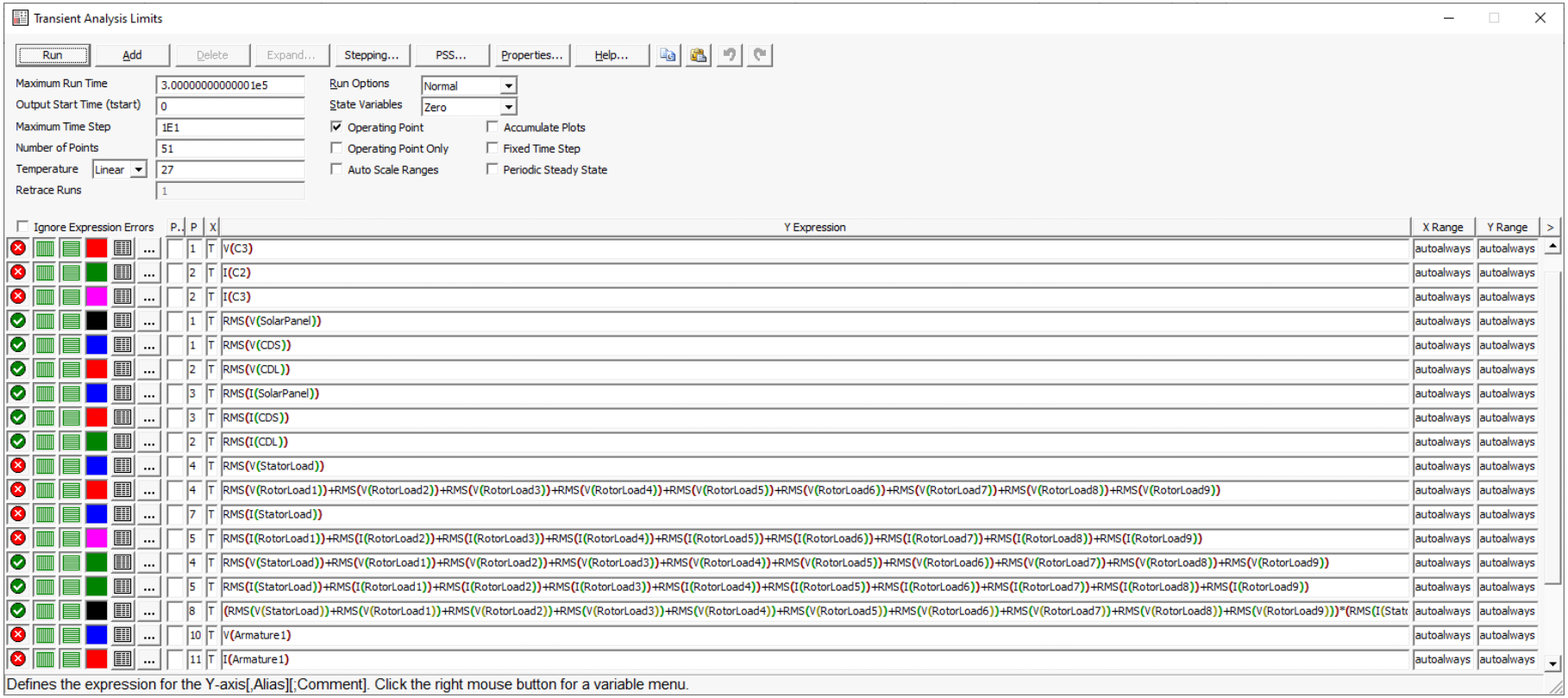

C < Welded > D
-3.027G
-3.027G
RotorLoad1
100m H
SJ14 SJ15
RotorLoad2
100m H
SJ16 SJ17
RotorLoad3
100m H
SJ18 SJ19
RotorLoad4
100m H
A
B
-3.027G
-3.027G
Simulation Max Time Step is 1e1
Magnetic Coupling #4
MotorLoad
C.Coef. .618
<< 10m Ohms using
<< parallel windings
Magnetic Coupling #1
IronCopper
C.Coef. .618
61.8% <= #1 <= 100%
#2 = sqr(100% – #1)
#3 = (100% – #1)^3
Magnetic Couplings #2
IronAluminum
C.Coef. .618
Iron_Aluminum
C.Coef. .618
Magnetic Coupling #3
CopperAluminum
C.Coef. .236
Copper_Aluminum
C.Coef. .236
StatorLoad
100 H
10 Ohms
C1
-2.682G
SJ1
SJ2
-2.682G
Junct
-6.521G
SJ5
SJ3
C2
-6.521G
Hint_Wrap the copper magnetic wire, completely covering it, with magnetic (VHS) video tape before winding it to the armature's bobbin.
Hint #2...
Oddly enough, it is the input of current, not the input of voltage, which gets in the way of the operation of this device which can either explode with wanton oblivion or else turn comatose on you. Both of these options must be prevented. Excess current from a larger voltage source can be thrown away to another ground connection via Current Division Large versus Current Division Small: CDL & CDS > > > > > > > > > > > > >
Ferrous Armature1 with 10H & 60 Ohms. Copper Coil on Bobbin is wrapped around the Armature.
SJ7
SJ8
-5.237G
Diode, must down-
D1
D1, point wards.
10 H
SJ9
SJ10
Ferrous Armature2 60 Ohms
61.8% = 2 ÷ {sqr(5) + 1}
Caps are 1e-13F & 3 Ohms ESR
SJ are solder joints @ 100m Ohms
CopperWireCageForTheAluminumDisks
embedded into the underside of the ferrous armature.
2u H
2µ Ohms
Junct
-6.521G
D2
Welded
This is a non-spinning locked stack of aluminum disks.
StackOfAluminumDisks
2m H
2m Ohms
C3
CDL
-29.745m
-2.704m
1 Ohm
SJ6
CDS
1.5e6
Ohms
Resistor, SJ31, is a short to prevent excessive voltage difference between both sides of the parallel rotor coils and maximize their current >>
1.5 V <<< The connection, of this voltage source, to ground must be welded – not soldered.
1.5
SolarPanel
Welded
or a Button Battery intended for Solar Powered Wallet (Credit Card Sized) Calculators.
A
B
SJ20
SJ21
RotorLoad5
100m H
SJ22
SJ23
RotorLoad6
100m H
SJ24
SJ25
RotorLoad7
100m H
SJ26
SJ27
RotorLoad8
100m H
SJ28
SJ29
RotorLoad9
100m H
C
D
SJ31
Nine rotor loads, connected in parallel, is the maximum before gain becomes a loss.
Magnetic Couplings #2
Armature1 StackOfAluminumDisks
Armature2 StackOfAluminumDisks
Magnetic Couplings #3
StatorLoad StackOfAluminumDisks
CopperWireCageForTheAluminumDisks StackOfAluminumDisks
Magnetic Coupling #1
StatorLoad Armature1 Armature2 CopperWireCageForTheAluminumDisks
Magnetic Coupling #4
StatorLoad RotorLoad1 RotorLoad2 RotorLoad3 RotorLoad4 RotorLoad5 RotorLoad6 RotorLoad7 RotorLoad8 RotorLoad9

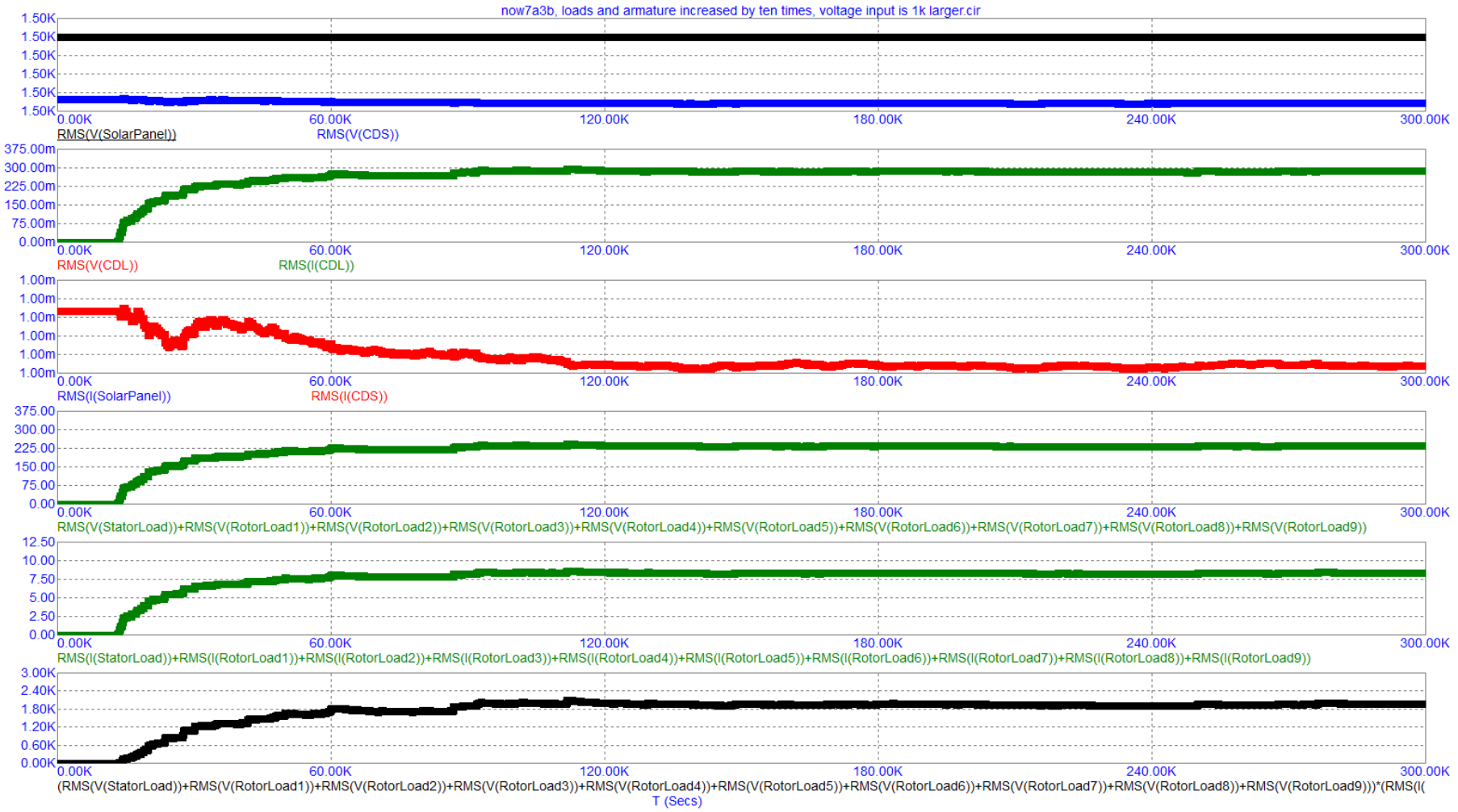
Schematic...

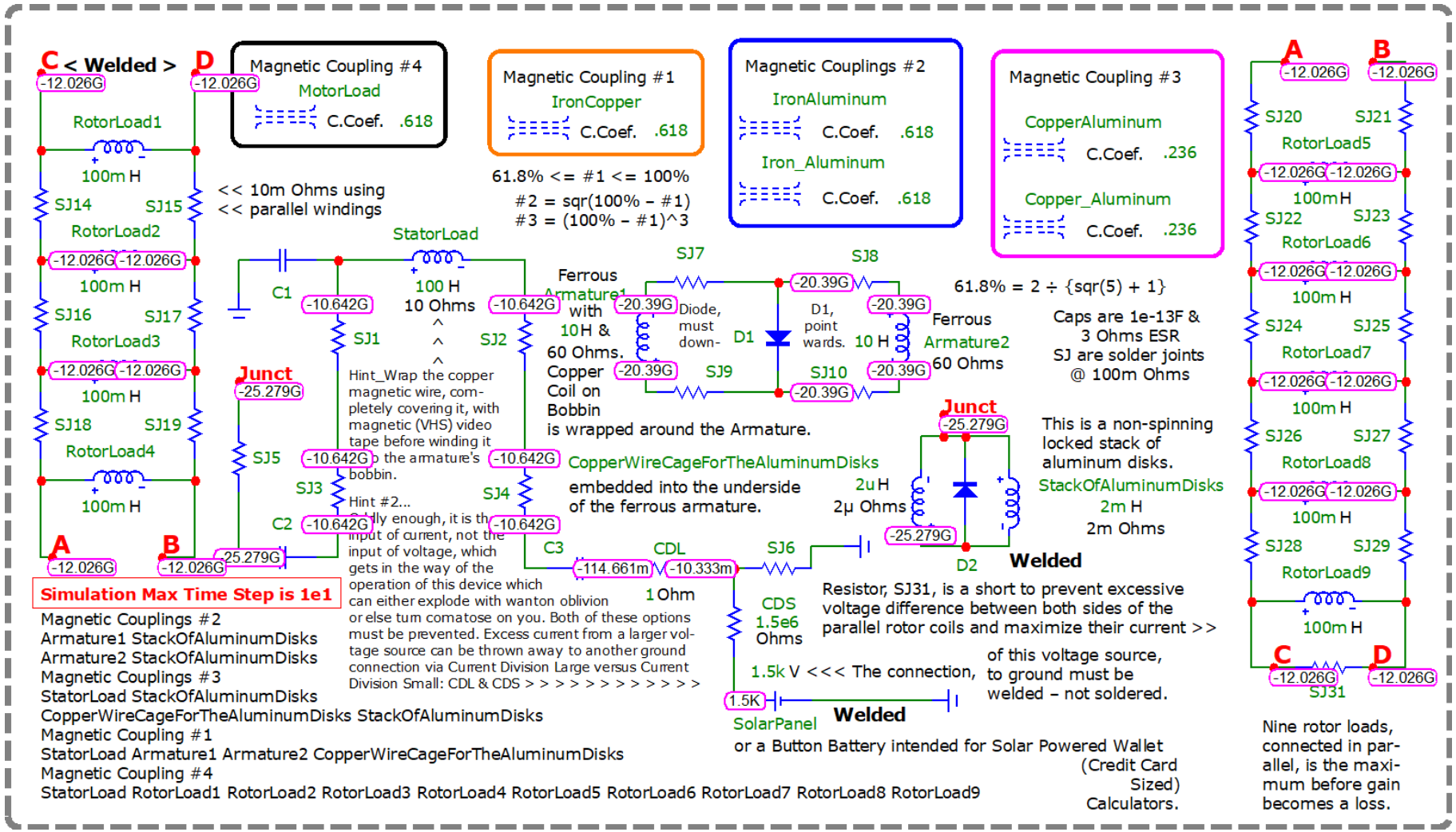


It doesn't matter whether I increase the voltage input by a factor of 1k...

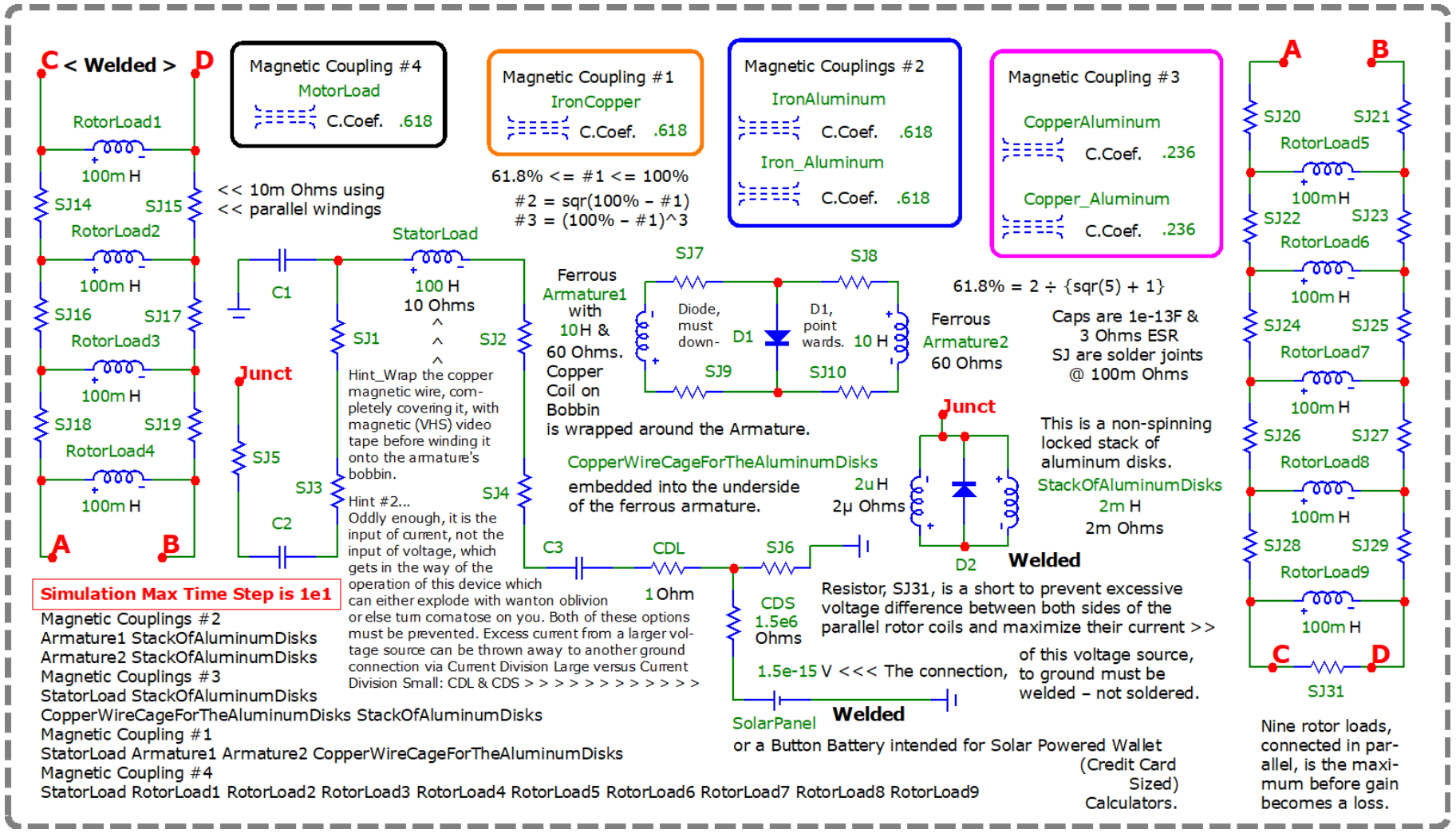

C < Welded > D
RotorLoad1
100m H
SJ14 SJ15
RotorLoad2
100m H
SJ16 SJ17
RotorLoad3
100m H
SJ18 SJ19
RotorLoad4
100m H
A B
Magnetic Coupling #4
MotorLoad
C.Coef. .618
<< 10m Ohms using
<< parallel windings
Magnetic Coupling #1
IronCopper
C.Coef. .618
61.8% <= #1 <= 100%
#2 = sqr(100% – #1)
#3 = (100% – #1)^3
Magnetic Couplings #2
IronAluminum
C.Coef. .618
Iron_Aluminum
C.Coef. .618
Magnetic Coupling #3
CopperAluminum
C.Coef. .236
Copper_Aluminum
C.Coef. .236
StatorLoad
C1
100 H
10 Ohms
SJ1 SJ2
Junct
SJ5
SJ3
SJ4
C2
Hint_Wrap the copper magnetic wire, completely covering it, with magnetic (VHS) video tape before winding it onto the armature's bobbin.
Hint #2...
Oddly enough, it is the input of current, not the input of voltage, which gets in the way of the operation of this device which can either explode with wanton oblivion or else turn comatose on you. Both of these options must be prevented. Excess current from a larger voltage source can be thrown away to another ground connection via Current Division Large versus Current Division Small: CDL & CDS > > > > > > > > > > > >
Ferrous Armature1 with 10H & 60 Ohms. Copper Coil on Bobbin is wrapped around the Armature.
SJ7 SJ8
Diode, must down- D1 D1, point wards. 10 H
SJ9 SJ10
Ferrous Armature2 60 Ohms
61.8% = 2 ÷ {sqr(5) + 1}
Caps are 1e-13F & 3 Ohms ESR
SJ are solder joints @ 100m Ohms
CopperWireCageForTheAluminumDisks
embedded into the underside of the ferrous armature.
2u H
2µ Ohms
Junct
D2
Welded
This is a non-spinning locked stack of aluminum disks.
StackOfAluminumDisks
2m H
2m Ohms
C3 CDL SJ6
1 Ohm
CDS 1.5e6 Ohms
Resistor, SJ31, is a short to prevent excessive voltage difference between both sides of the parallel rotor coils and maximize their current >>
1.5k V <<< The connection, of this voltage source, to ground must be welded – not soldered.
SolarPanel
Welded
or a Button Battery intended for Solar Powered Wallet (Credit Card Sized) Calculators.
A B
SJ20 SJ21
RotorLoad5
100m H
SJ22 SJ23
RotorLoad6
100m H
SJ24 SJ25
RotorLoad7
100m H
SJ26 SJ27
RotorLoad8
100m H
SJ28 SJ29
RotorLoad9
100m H
C D
SJ31
Nine rotor loads, connected in parallel, is the maximum before gain becomes a loss.
Simulation Max Time Step is 1e1
Magnetic Couplings #2
Armature1 StackOfAluminumDisks
Armature2 StackOfAluminumDisks
Magnetic Couplings #3
StatorLoad StackOfAluminumDisks
CopperWireCageForTheAluminumDisks StackOfAluminumDisks
Magnetic Coupling #1
StatorLoad Armature1 Armature2 CopperWireCageForTheAluminumDisks
Magnetic Coupling #4
StatorLoad RotorLoad1 RotorLoad2 RotorLoad3 RotorLoad4 RotorLoad5 RotorLoad6 RotorLoad7 RotorLoad8 RotorLoad9

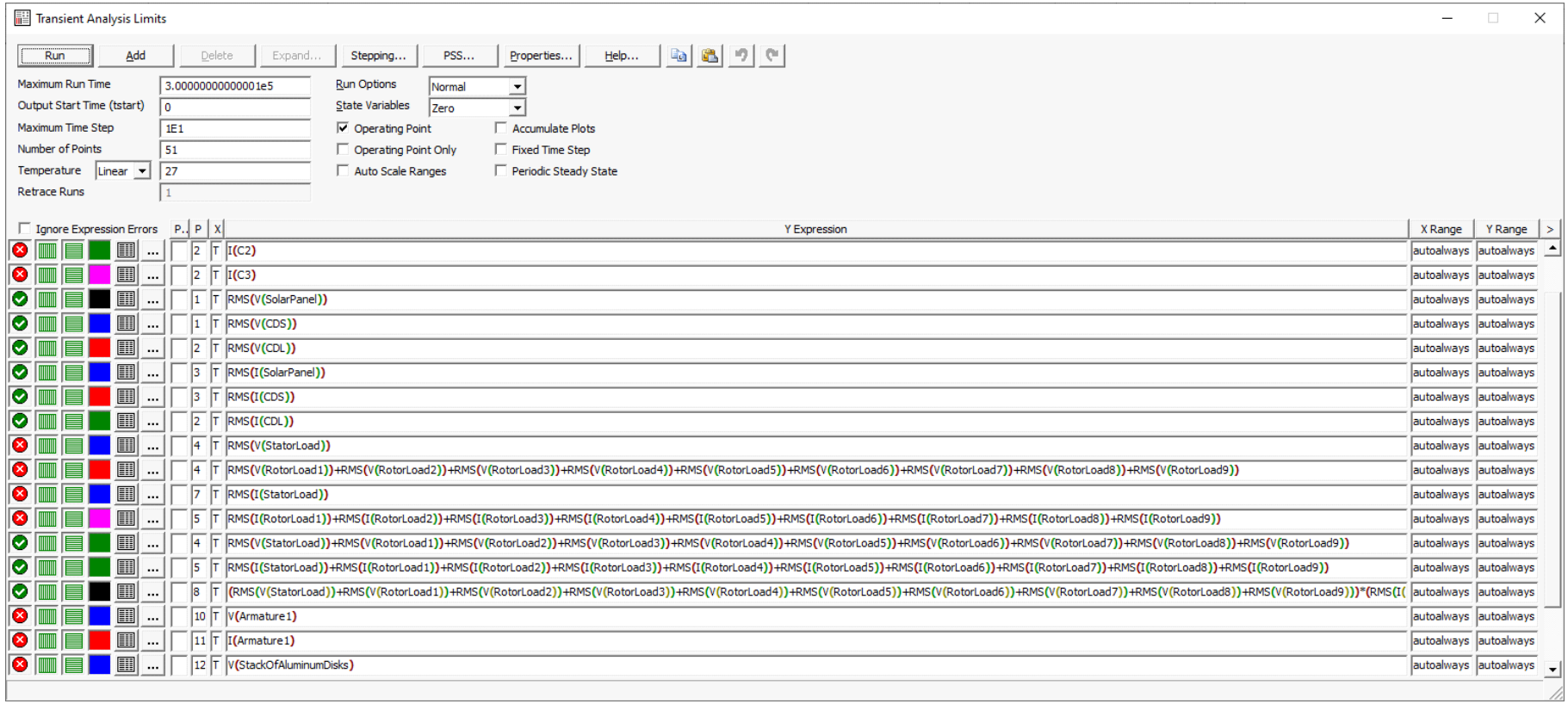

Transient Analysis Limits
Run
Add
Delete
Expand...
Stepping...
PSS...
Properties...
Help...
Maximum Run Time
3.000000000000001e5
Output Start Time (tstart)
0
Maximum Time Step
1E1
Number of Points
51
Temperature
Linear
27
Retrace Runs
1
Run Options
Normal
State Variables
Zero
Operating Point
Operating Point Only
Auto Scale Ranges
Accumulate Plots
Fixed Time Step
Periodic Steady State
Ignore Expression Errors
P..
P
X
Y Expression
X Range
Y Range
V(C3)
I(C2)
I(C3)
RMS(V(SolarPanel))
RMS(V(CDS))
RMS(V(CDL))
RMS(I(SolarPanel))
RMS(I(CDS))
RMS(I(CDL))
RMS(V(StatorLoad))
RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9))
RMS(I(StatorLoad))
RMS(I(RotorLoad1))+RMS(I(RotorLoad2))+RMS(I(RotorLoad3))+RMS(I(RotorLoad4))+RMS(I(RotorLoad5))+RMS(I(RotorLoad6))+RMS(I(RotorLoad7))+RMS(I(RotorLoad8))+RMS(I(RotorLoad9))
RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9))
RMS(I(StatorLoad))+RMS(I(RotorLoad1))+RMS(I(RotorLoad2))+RMS(I(RotorLoad3))+RMS(I(RotorLoad4))+RMS(I(RotorLoad5))+RMS(I(RotorLoad6))+RMS(I(RotorLoad7))+RMS(I(RotorLoad8))+RMS(I(RotorLoad9))
(RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9)))*(RMS(I(Stat
V(Armature1)
I(Armature1)
autoalways
Defines the expression for the Y-axis[,Alias][;Comment]. Click the right mouse button for a variable menu.

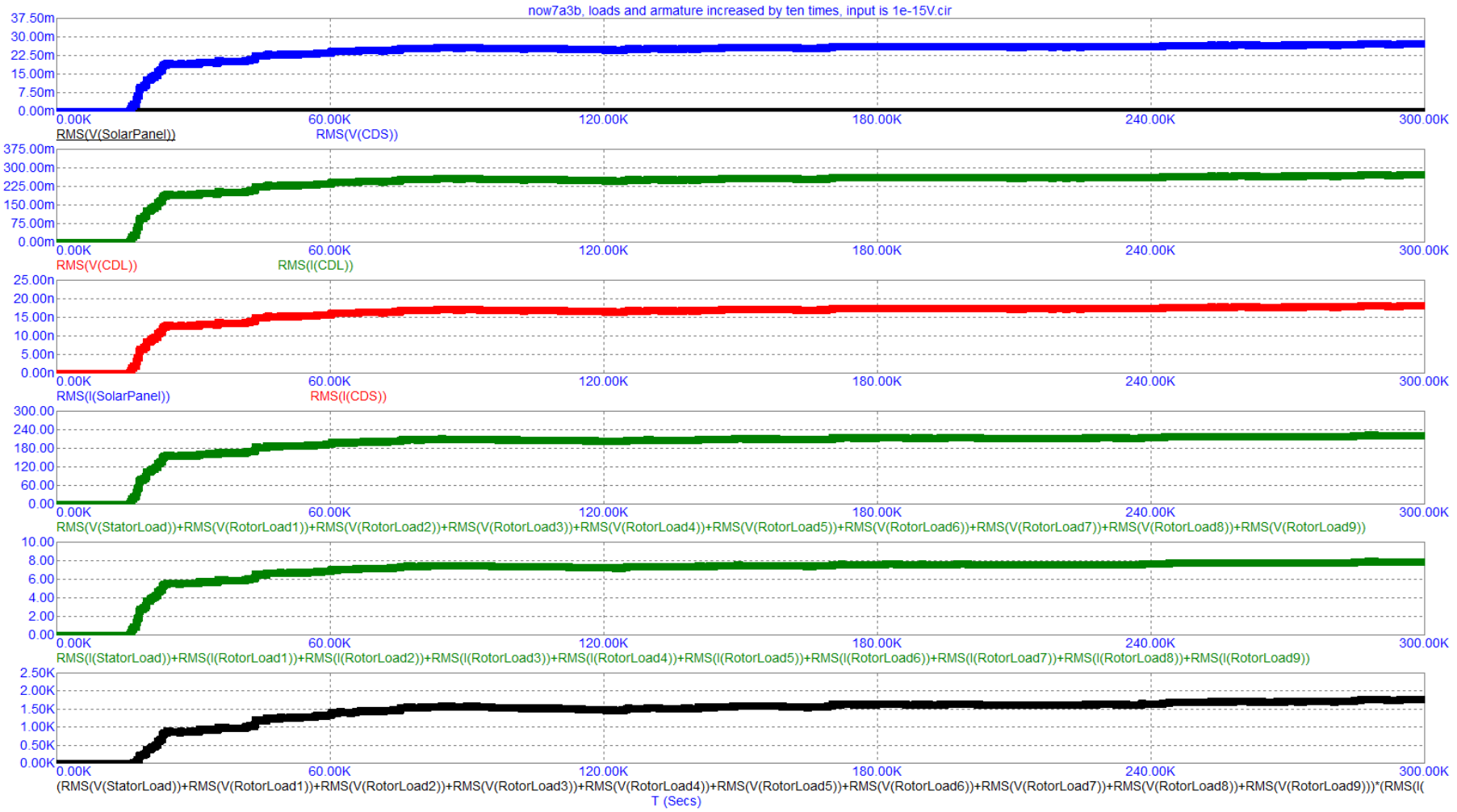

now7a3b, loads and armature increased by ten times, voltage input is 1k larger.cir
1.50K
1.50K
1.50K
1.50K
1.50K
1.50K
0.00K
60.00K
120.00K
180.00K
240.00K
300.00K
RMS(V(SolarPanel))
RMS(V(CDS))
375.00m
300.00m
225.00m
150.00m
75.00m
0.00m
0.00K
60.00K
120.00K
180.00K
240.00K
300.00K
RMS(V(CDL))
RMS(I(CDL))
1.00m
1.00m
1.00m
1.00m
1.00m
1.00m
0.00K
60.00K
120.00K
180.00K
240.00K
300.00K
RMS(I(SolarPanel))
RMS(I(CDS))
375.00
300.00
225.00
150.00
75.00
0.00
0.00K
60.00K
120.00K
180.00K
240.00K
300.00K
RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9))
12.50
10.00
7.50
5.00
2.50
0.00
0.00K
60.00K
120.00K
180.00K
240.00K
300.00K
RMS(I(StatorLoad))+RMS(I(RotorLoad1))+RMS(I(RotorLoad2))+RMS(I(RotorLoad3))+RMS(I(RotorLoad4))+RMS(I(RotorLoad5))+RMS(I(RotorLoad6))+RMS(I(RotorLoad7))+RMS(I(RotorLoad8))+RMS(I(RotorLoad9))
3.00K
2.40K
1.80K
1.20K
0.60K
0.00K
0.00K
60.00K
120.00K
180.00K
240.00K
300.00K
(RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9)))*(RMS(I(
T (Secs)

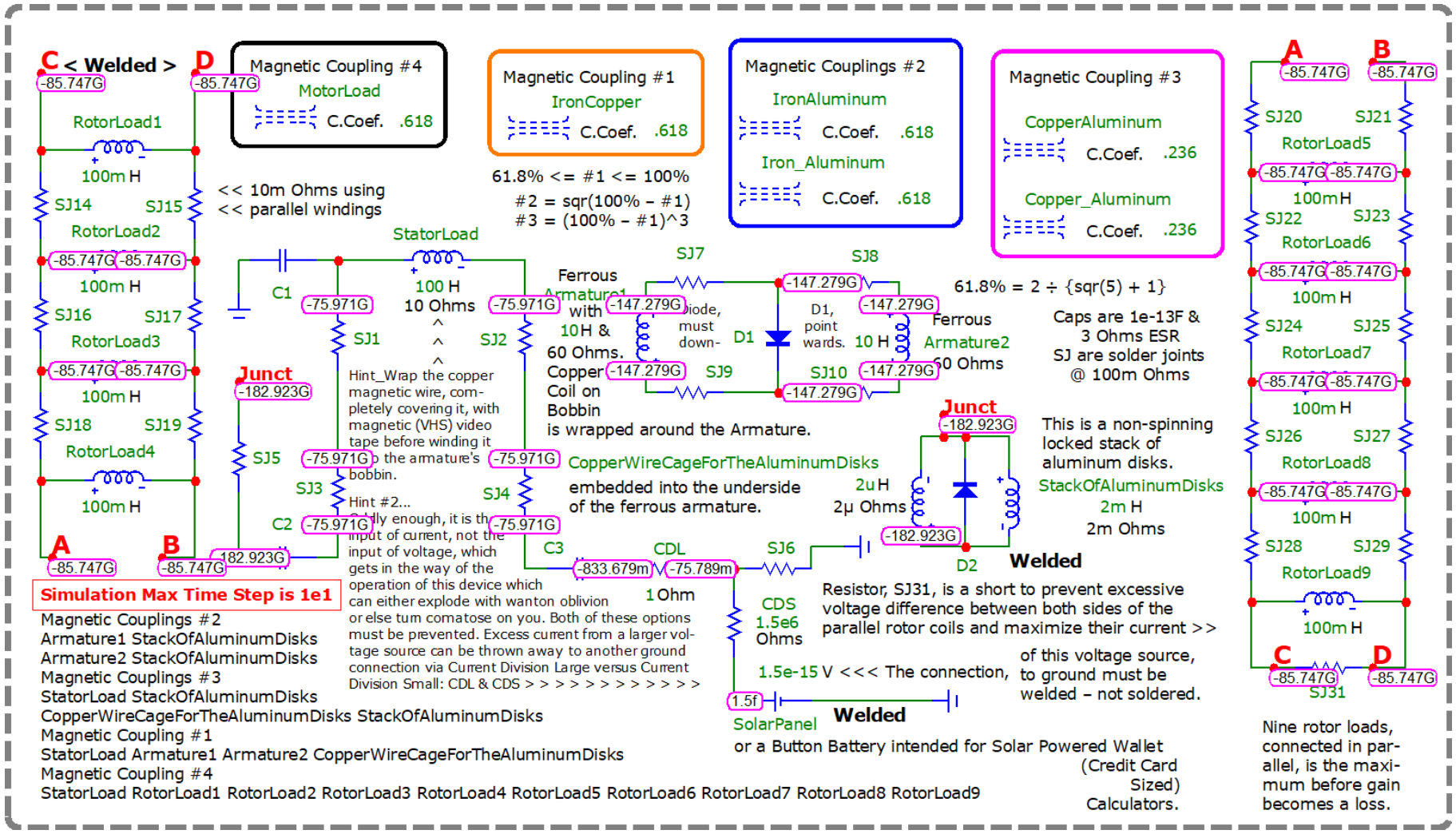


Nor does it matter whether I reduce the voltage input to 1.5e-15V...


C < Welded > D
RotorLoad1
100m H
SJ14 SJ15
RotorLoad2
100m H
SJ16 SJ17
RotorLoad3
100m H
SJ18 SJ19
RotorLoad4
100m H
A B
Magnetic Coupling #4
MotorLoad
C.Coef. .618
<< 10m Ohms using
<< parallel windings
Magnetic Coupling #1
IronCopper
C.Coef. .618
61.8% <= #1 <= 100%
#2 = sqr(100% – #1)
#3 = (100% – #1)^3
Magnetic Couplings #2
IronAluminum
C.Coef. .618
Iron_Aluminum
C.Coef. .618
Magnetic Coupling #3
CopperAluminum
C.Coef. .236
Copper_Aluminum
C.Coef. .236
StatorLoad
C1
100 H
10 Ohms
SJ1
SJ2
Junct
SJ5
SJ3
C2
Hint_Wrap the copper magnetic wire, completely covering it, with magnetic (VHS) video tape before winding it onto the armature's bobbin.
Hint #2...
Oddly enough, it is the input of current, not the input of voltage, which gets in the way of the operation of this device which can either explode with wanton oblivion or else turn comatose on you. Both of these options must be prevented. Excess current from a larger voltage source can be thrown away to another ground connection via Current Division Large versus Current Division Small: CDL & CDS > > > > > > > > > > > > >
Ferrous Armature1 with 10H & 60 Ohms. Copper Coil on Bobbin is wrapped around the Armature.
SJ7
SJ8
Diode, must down-
D1
D1, point wards.
10 H
SJ9
SJ10
Ferrous Armature2 60 Ohms
61.8% = 2 ÷ {sqr(5) + 1}
Caps are 1e-13F & 3 Ohms ESR
SJ are solder joints @ 100m Ohms
CopperWireCageForTheAluminumDisks
embedded into the underside of the ferrous armature.
2u H
2µ Ohms
Junct
D2
Welded
This is a non-spinning locked stack of aluminum disks.
StackOfAluminumDisks
2m H
2m Ohms
C3
CDL
1 Ohm
SJ6
SJ4
CDS
1.5e6
Ohms
Resistor, SJ31, is a short to prevent excessive voltage difference between both sides of the parallel rotor coils and maximize their current >>
1.5e-15 V <<< The connection, of this voltage source, to ground must be welded – not soldered.
SolarPanel
Welded
or a Button Battery intended for Solar Powered Wallet (Credit Card Sized) Calculators.
A B
SJ20 SJ21
RotorLoad5
100m H
SJ22 SJ23
RotorLoad6
100m H
SJ24 SJ25
RotorLoad7
100m H
SJ26 SJ27
RotorLoad8
100m H
SJ28 SJ29
RotorLoad9
100m H
C D
SJ31
Nine rotor loads, connected in parallel, is the maximum before gain becomes a loss.
Simulation Max Time Step is 1e1
Magnetic Couplings #2
Armature1 StackOfAluminumDisks
Armature2 StackOfAluminumDisks
Magnetic Couplings #3
StatorLoad StackOfAluminumDisks
CopperWireCageForTheAluminumDisks StackOfAluminumDisks
Magnetic Coupling #1
StatorLoad Armature1 Armature2 CopperWireCageForTheAluminumDisks
Magnetic Coupling #4
StatorLoad RotorLoad1 RotorLoad2 RotorLoad3 RotorLoad4 RotorLoad5 RotorLoad6 RotorLoad7 RotorLoad8 RotorLoad9


Transient Analysis Limits
Run
Add
Delete
Expand...
Stepping...
PSS...
Properties...
Help...
Maximum Run Time
3.000000000000001e5
Output Start Time (tstart)
0
Maximum Time Step
1E1
Number of Points
51
Temperature
Linear
27
Retrace Runs
1
Run Options
Normal
State Variables
Zero
Operating Point
Operating Point Only
Auto Scale Ranges
Accumulate Plots
Fixed Time Step
Periodic Steady State
Ignore Expression Errors
P..
P
X
Y Expression
X Range
Y Range
2 T I(C2) autoalways autoalways
2 T I(C3) autoalways autoalways
1 T RMS(V(SolarPanel)) autoalways autoalways
1 T RMS(V(CDS)) autoalways autoalways
2 T RMS(V(CDL)) autoalways autoalways
3 T RMS(I(SolarPanel)) autoalways autoalways
3 T RMS(I(CDS)) autoalways autoalways
2 T RMS(I(CDL)) autoalways autoalways
4 T RMS(V(StatorLoad)) autoalways autoalways
4 T RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9)) autoalways autoalways
7 T RMS(I(StatorLoad)) autoalways autoalways
5 T RMS(I(RotorLoad1))+RMS(I(RotorLoad2))+RMS(I(RotorLoad3))+RMS(I(RotorLoad4))+RMS(I(RotorLoad5))+RMS(I(RotorLoad6))+RMS(I(RotorLoad7))+RMS(I(RotorLoad8))+RMS(I(RotorLoad9)) autoalways autoalways
4 T RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9)) autoalways autoalways
5 T RMS(I(StatorLoad))+RMS(I(RotorLoad1))+RMS(I(RotorLoad2))+RMS(I(RotorLoad3))+RMS(I(RotorLoad4))+RMS(I(RotorLoad5))+RMS(I(RotorLoad6))+RMS(I(RotorLoad7))+RMS(I(RotorLoad8))+RMS(I(RotorLoad9)) autoalways autoalways
8 T (RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9)))*(RMS(I(autoalways autoalways
10 T V(Armature1) autoalways autoalways
11 T I(Armature1) autoalways autoalways
12 T V(StackOfAluminumDisks) autoalways autoalways


now7a3b, loads and armature increased by ten times, input is 1e-15V.cir
37.50m
30.00m
22.50m
15.00m
7.50m
0.00m
0.00K
60.00K
120.00K
180.00K
240.00K
300.00K
RMS(V(SolarPanel))
RMS(V(CDS))
375.00m
300.00m
225.00m
150.00m
75.00m
0.00m
RMS(V(CDL))
RMS(I(CDL))
25.00n
20.00n
15.00n
10.00n
5.00n
0.00n
RMS(I(SolarPanel))
RMS(I(CDS))
300.00
240.00
180.00
120.00
60.00
0.00
RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9))
10.00
8.00
6.00
4.00
2.00
0.00
RMS(I(StatorLoad))+RMS(I(RotorLoad1))+RMS(I(RotorLoad2))+RMS(I(RotorLoad3))+RMS(I(RotorLoad4))+RMS(I(RotorLoad5))+RMS(I(RotorLoad6))+RMS(I(RotorLoad7))+RMS(I(RotorLoad8))+RMS(I(RotorLoad9))
2.50K
2.00K
1.50K
1.00K
0.50K
0.00K
(RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9)))*(RMS(I(
T (Secs)



The end result is roughly the same! Now, that's a stable circuit topology for ya!

But it has been stabilized, up above, to avoid a reactive explosion and a simulator error of: “time step too small for transient analysis” by performing a bit of trickery...

The maximum time step during simulation has been raised above the simulator's default condition of zero to a considerable amount from as little as ten seconds (1E1) to as much as one thousand seconds (1E3).

By thinking a little about this challenge, I determined (correctly) that the problem lay in too much armature inductance producing too much power for the stator and rotor loads to consume. This would be exactly the same as if our Sun were significantly larger in its output than it presently is, or if we suddenly lost a planet such as what happened many hundreds of thousands of years ago when the planet Maldek blew up in between the orbits of Mars and Jupiter resulting in the current comet belt between those two planets. This was due to a crazy scientist's project which went awry after his death through mismanagement and was electrically compensated by the insertion of a new planet, Earth, taken from the Pleiades galaxy.[19] *{Who did this? Maybe, God, or his angelic administration of His government?}* So, for this circuit, all I had to do was lower the armature inductance by 70% from a value of one Henry to a value of 700 milli- Henrys and also reduce the resistance of these inductances from a value of 6 Ohms (representing the resistance of iron wire) to a value of 4.2 Ohms (70% of 6 Ohms) to prevent an explosion of power and a simulator error whenever running a transient analysis at a zero maximum time step. I also had to limit the resistance of the two solder joints which flank either side of the stator load to a maximum value of 240 milli-Ohms. Otherwise, at 250 milli-Ohms for each resistor, an explosion of energy occurs.

I suspect that stipulating a maximum time step greater than zero injects a certain amount of “fuzzy logic”. This is less precise than specifying a zero maximum time step. A zero maximum time step lets the simulator pick its own series of maximum time steps as per whatever it sees fit at each moment during its runtime. I think that fuzzy logic implies less accuracy. This is why I sought to reduce the size of the armature's inductance since I reasoned that I had failed to prevent an explosion of power since this is what happens at a zero maximum time step and one Henry per armature “coil”. In other words, the supply of reactive power coming from the armature was too much for the stator and rotor loads to consume. Since the load is fixed in my circuit by the size of the stator coils of an electric vehicle's motors at ten Henrys and its rotors are fixed at 100 milli-Henrys, for each rotor coil, then my only option is to reduce the reactive supply coming from the armature.

I know I sound like I am repeating myself. But this is to insure I get the point across that power is coming from the reactance of this circuit's components. It is NOT coming from the so-called power supply (the battery representing a solar panel). This defies conventional logic and the “acceptable” laws of physics, but so what? They're wrong some of the time...

As I told an electrical engineer...

Energy does not travel down the wire. Only if the atoms of copper (in a copper wire) were to move down the length of a piece of wire or a coil, only then would the valence electrons in orbit around each copper atom move as well. Otherwise, the valence electrons stay in place and change their energetic state, up or down, in series of changes running down the length of a piece of wire creating a pattern (in the shape of a ripple) which we mistakenly judge to be a wave of energy. It is not. It is a waveform representing the atomic transference of information among the valence electrons in orbit around the nucleus of their atoms of copper to which they belong and adhere to. This transference is a serial movement down the length of the wire giving the illusion that something substantial is moving, such as: massless photons (what a joke!).

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19 Mentioned to those of us who visited Charlie Lutes' advanced lectures given to Transcendental Meditators. See, http://w.charlielutes.info/

Atoms of copper are conscientious. They are conscious of their surroundings, namely: the voltage parameter of each of their neighboring atoms of copper. They respond to changes in the voltages of their neighbors due to their cross-linkages occurring among their valence electrons when the copper ore was melted into a solid piece of wire.

It is like a circle of people holding hands creating a chained linkage which affects everyone as a group. If one person moves, then everyone else feels the tug while everyone remains standing in place without walking anywhere. This is what the movement of energy amounts to: a communication of a changing energetic state of valence electrons. It is like people doing "the wave" out of boredom at a football game[20] by standing up and raising their arms and sitting down and lowering their arms. Only if they had gotten up and run around the stadium during half-time until the music stopped playing and then immediately sat down[21] would this constitute the actual movement of their dynamic (living) bodies and what this dynamism implies: energetic life.

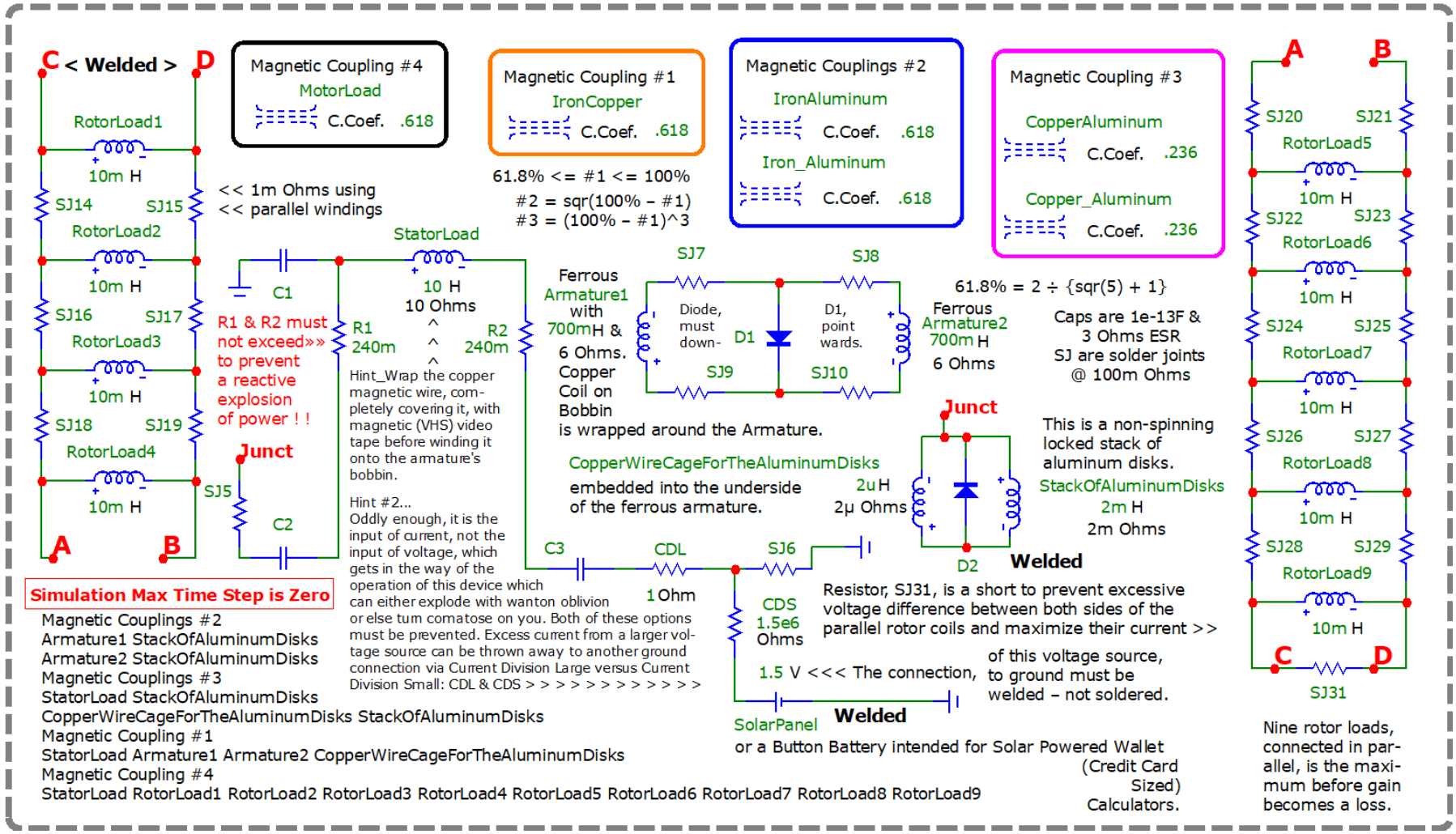
At no time while "the wave" travels around the stadium does energy rotate around the stadium.[22] Only a ripple,[23] which we recognize from a suitable distance of "fuzzy perspective", travels around the stadium representing the movement of people's reaction to the approach of this ripple as it arrives to them and passes them by.

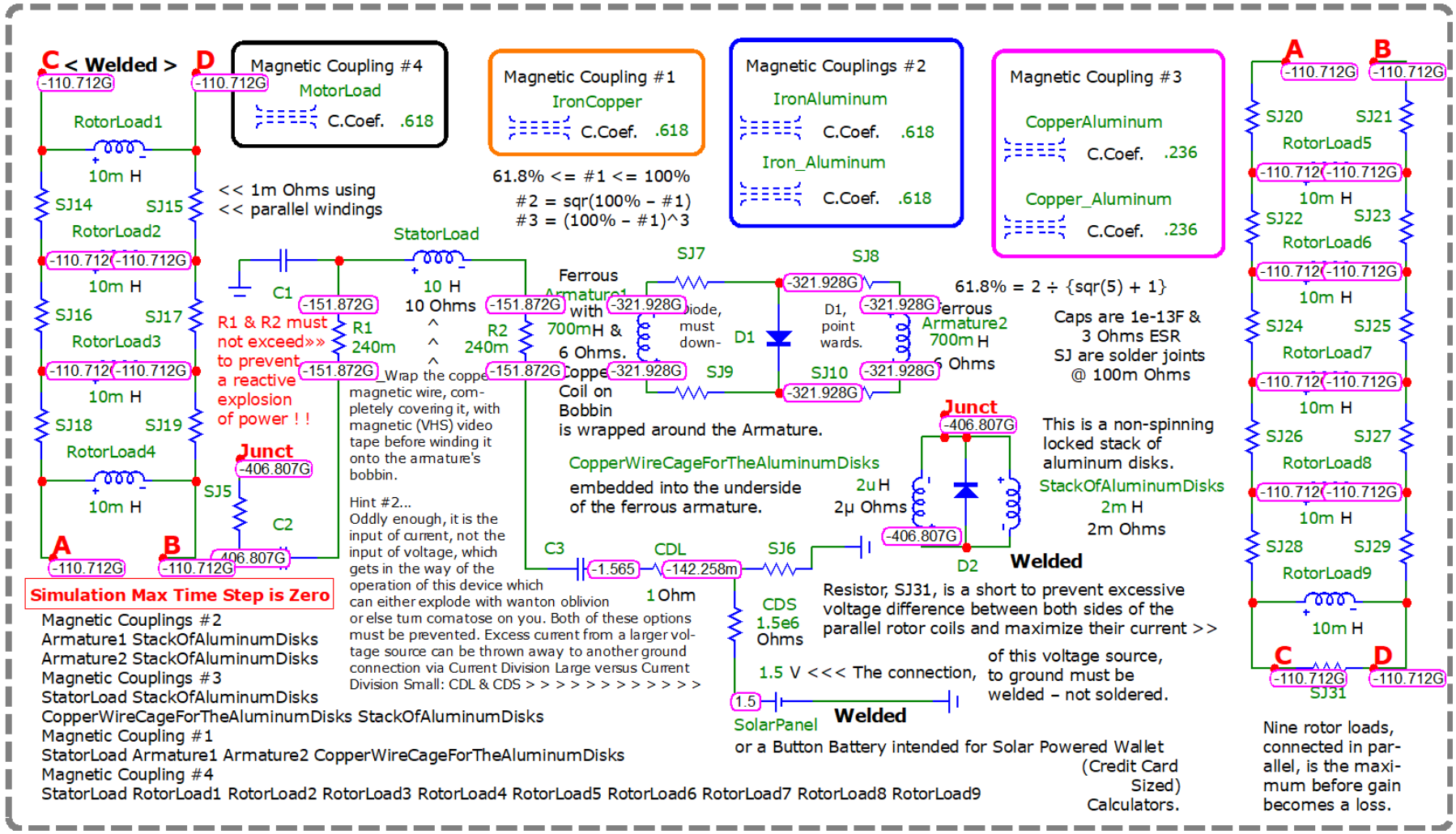
No planet in its right mind would scoot around the universe. It sits in orbit around its respective star. The valence electrons of atoms of the materials of construction within a circuit are no different than planets in orbit around a star.

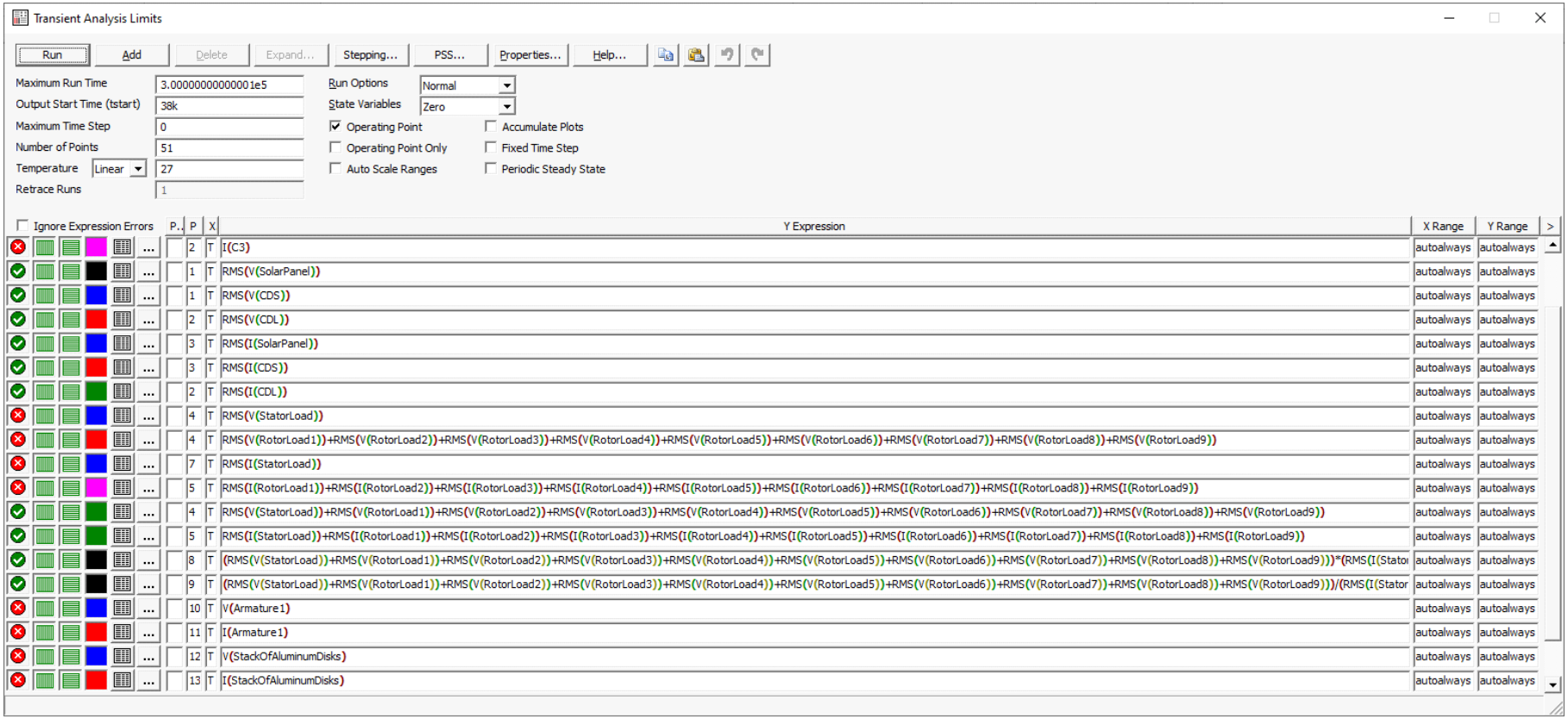
Also, please make note of this fact: that the armature is *not* a pair of coils. The armature is a solid core of ferromagnetizable (iron) around which the stator is wound. I had to give this armature a pair of fictional coils in order to endow its solid construction (of core material) with an inductance which the simulator can appreciate.

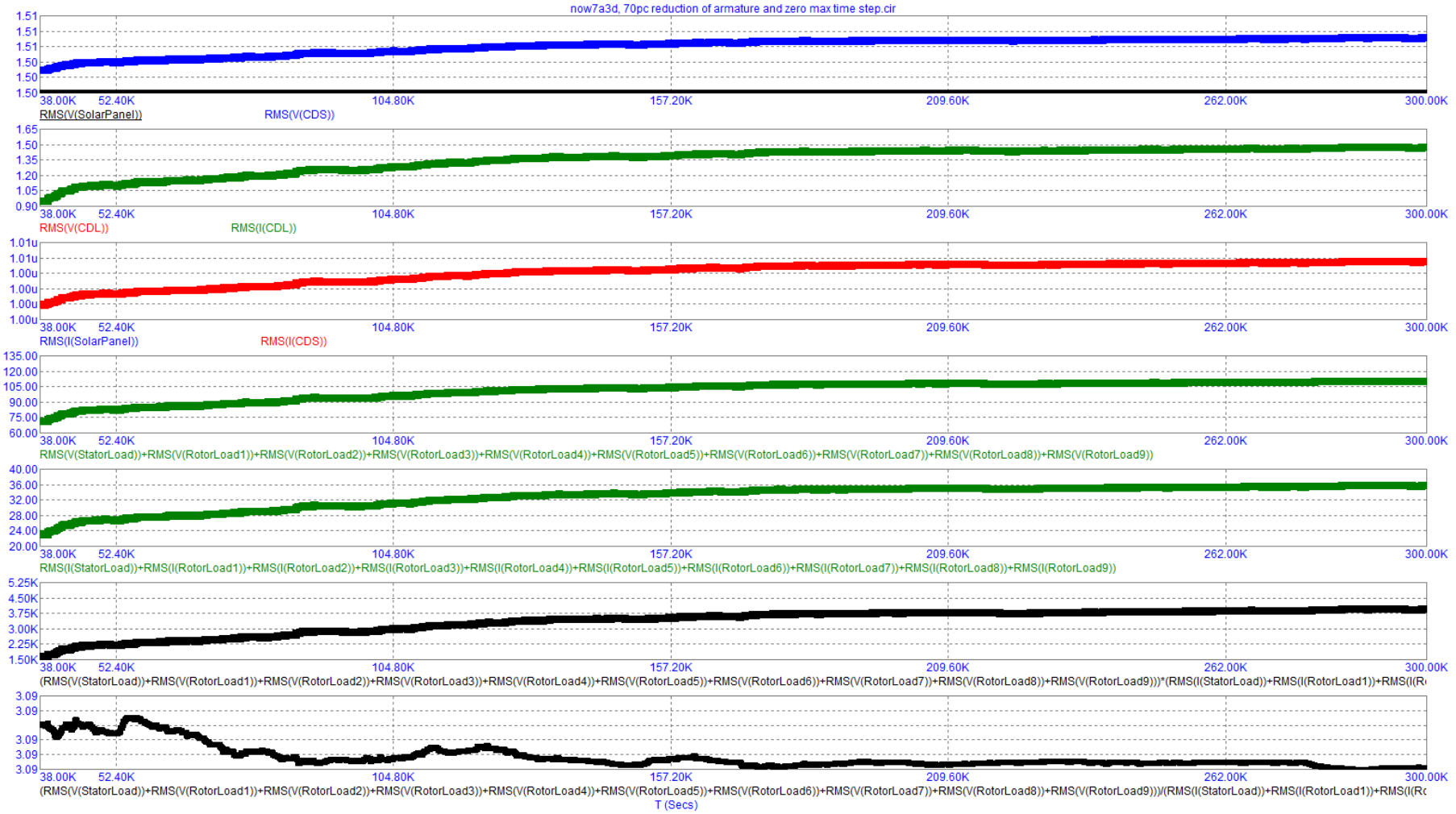
Here are the modifications to possibly achieve a more buildable circuit (which is more realistic)...

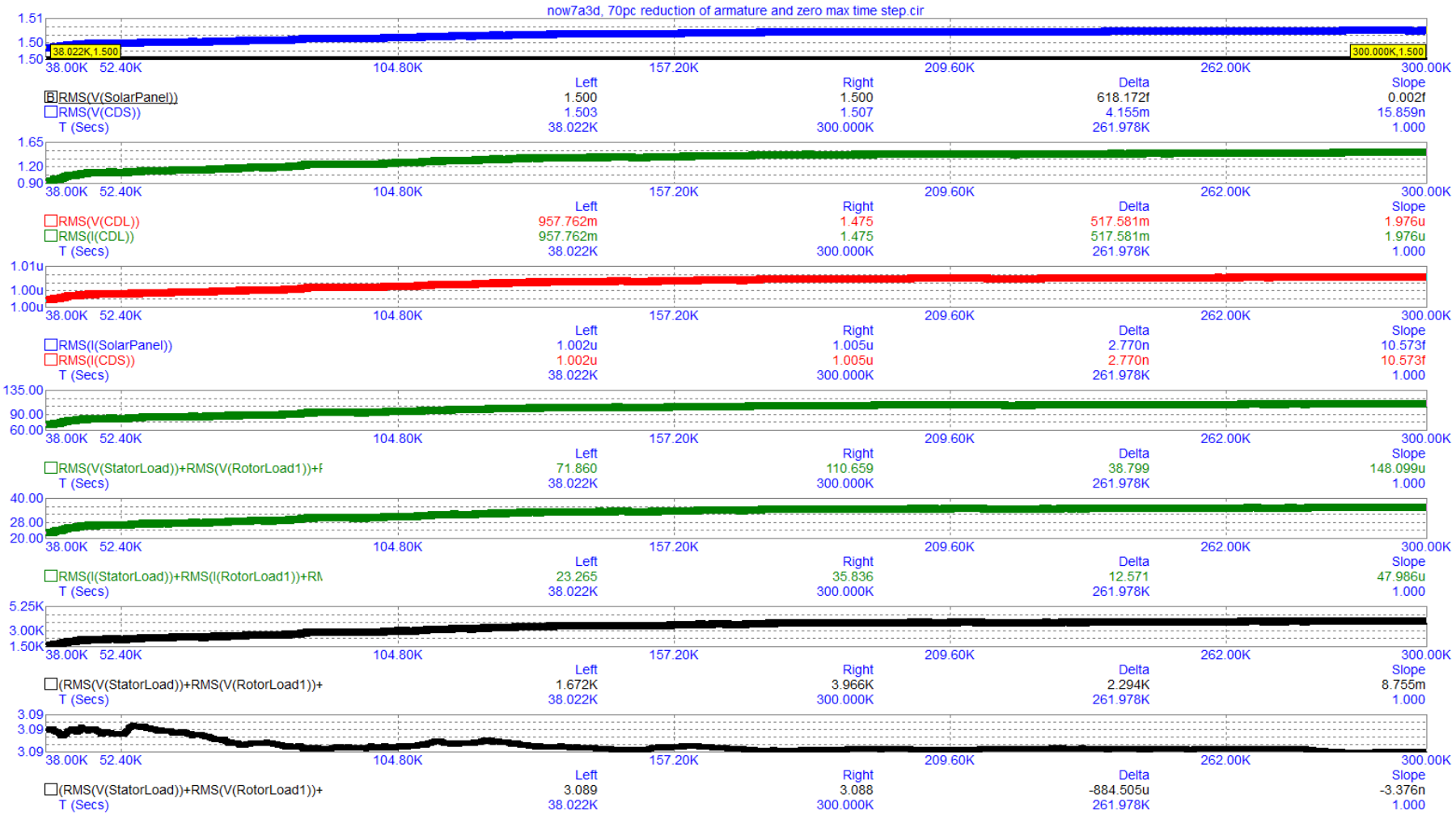
20 https://en.wikipedia.org/wiki/Wave_%28audience%29
21 https://duckduckgo.com/?q=musical+chairs+game+description&ia=web
22 https://www.youtube.com/watch?v=OI_HFnNTfyU&t=607
23 https://en.wikipedia.org/wiki/Metachronal_rhythm


C < Welded > D
RotorLoad1
10m H
SJ14
SJ15
RotorLoad2
10m H
SJ16
SJ17
RotorLoad3
10m H
SJ18
SJ19
RotorLoad4
10m H
SJ5
A
B
Magnetic Coupling #4
MotorLoad
C.Coef. .618
<< 1m Ohms using
<< parallel windings
C1
R1 & R2 must not exceed»» to prevent a reactive explosion of power ! !
Junct
C2
StatorLoad
10 H
10 Ohms
R1
240m
R2
240m
Hint_Wrap the copper magnetic wire, completely covering it, with magnetic (VHS) video tape before winding it onto the armature's bobbin.
Hint #2...
Oddly enough, it is the input of current, not the input of voltage, which gets in the way of the operation of this device which can either explode with wanton oblivion or else turn comatose on you. Both of these options must be prevented. Excess current from a larger voltage source can be thrown away to another ground connection via Current Division Large versus Current Division Small: CDL & CDS > > > > > > > > > > > > >
Magnetic Coupling #1
IronCopper
C.Coef. .618
61.8% <= #1 <= 100%
#2 = sqr(100% – #1)
#3 = (100% – #1)^3
Magnetic Couplings #2
IronAluminum
C.Coef. .618
Iron_Aluminum
C.Coef. .618
Magnetic Coupling #3
CopperAluminum
C.Coef. .236
Copper_Aluminum
C.Coef. .236
SJ7
SJ8
Ferrous Armature1 with 700mH & 6 Ohms. Copper Coil on Bobbin is wrapped around the Armature.
Diode, must down-
D1
D1, point wards.
SJ9
SJ10
Ferrous Armature2 700m H 6 Ohms
61.8% = 2 ÷ {sqr(5) + 1}
Caps are 1e-13F & 3 Ohms ESR
SJ are solder joints @ 100m Ohms
CopperWireCageForTheAluminumDisks
embedded into the underside of the ferrous armature.
2u H
2µ Ohms
Junct
D2
Welded
This is a non-spinning locked stack of aluminum disks.
StackOfAluminumDisks
2m H
2m Ohms
C3
CDL
1 Ohm
SJ6
CDS
1.5e6
Ohms
Resistor, SJ31, is a short to prevent excessive voltage difference between both sides of the parallel rotor coils and maximize their current >>
1.5 V <<< The connection, of this voltage source, to ground must be welded – not soldered.
SolarPanel
Welded
or a Button Battery intended for Solar Powered Wallet (Credit Card Sized) Calculators.
A
B
SJ20
SJ21
RotorLoad5
10m H
SJ22
SJ23
RotorLoad6
10m H
SJ24
SJ25
RotorLoad7
10m H
SJ26
SJ27
RotorLoad8
10m H
SJ28
SJ29
RotorLoad9
10m H
C
D
SJ31
Nine rotor loads, connected in parallel, is the maximum before gain becomes a loss.
Simulation Max Time Step is Zero
Magnetic Couplings #2
Armature1 StackOfAluminumDisks
Armature2 StackOfAluminumDisks
Magnetic Couplings #3
StatorLoad StackOfAluminumDisks
CopperWireCageForTheAluminumDisks StackOfAluminumDisks
Magnetic Coupling #1
StatorLoad Armature1 Armature2 CopperWireCageForTheAluminumDisks
Magnetic Coupling #4
StatorLoad RotorLoad1 RotorLoad2 RotorLoad3 RotorLoad4 RotorLoad5 RotorLoad6 RotorLoad7 RotorLoad8 RotorLoad9


C < Welded >
D
-110.712G
-110.712G
Magnetic Coupling #4
MotorLoad
C.Coef. .618
Magnetic Coupling #1
IronCopper
C.Coef. .618
61.8% <= #1 <= 100%
#2 = sqr(100% – #1)
#3 = (100% – #1)^3
Magnetic Couplings #2
IronAluminum
C.Coef. .618
Iron_Aluminum
C.Coef. .618
Magnetic Coupling #3
CopperAluminum
C.Coef. .236
Copper_Aluminum
C.Coef. .236
RotorLoad1
10m H
SJ14
SJ15
<< 1m Ohms using
<< parallel windings
RotorLoad2
10m H
SJ16
SJ17
RotorLoad3
10m H
SJ18
SJ19
RotorLoad4
10m H
A
B
-110.712G
-110.712G
StatorLoad
10 H
10 Ohms
C1
-151.872G
R1
240m
R2
240m
-151.872G
-151.872G
R1 & R2 must not exceed»» to prevent a reactive explosion of power ! !
Junct
-406.807G
SJ5
C2
-406.807G
Ferrous Armature1 with 700mH & 6 Ohms.
SJ7
SJ8
-321.928G
-321.928G
-321.928G
-321.928G
-321.928G
-321.928G
SJ9
SJ10
D1
Diode, must down-
D1, point wards.
Ferrous Armature2 700m H
6 Ohms
61.8% = 2 ÷ {sqr(5) + 1}
Caps are 1e-13F & 3 Ohms ESR
SJ are solder joints @ 100m Ohms
Coil on Bobbin is wrapped around the Armature.
Wrap the copper magnetic wire, completely covering it, with magnetic (VHS) video tape before winding it onto the armature's bobbin.
Hint #2...
Oddly enough, it is the input of current, not the input of voltage, which gets in the way of the operation of this device which can either explode with wanton oblivion or else turn comatose on you. Both of these options must be prevented. Excess current from a larger voltage source can be thrown away to another ground connection via Current Division Large versus Current Division Small: CDL & CDS > > > > > > > > > > > > >
CopperWireCageForTheAluminumDisks
embedded into the underside of the ferrous armature.
2u H
2µ Ohms
Junct
-406.807G
-406.807G
D2
This is a non-spinning locked stack of aluminum disks.
StackOfAluminumDisks
2m H
2m Ohms
Welded
C3
CDL
SJ6
-1.565
-142.258m
1 Ohm
CDS
1.5e6
Ohms
Resistor, SJ31, is a short to prevent excessive voltage difference between both sides of the parallel rotor coils and maximize their current >>
1.5 V <<< The connection, of this voltage source, to ground must be welded – not soldered.
1.5
SolarPanel
Welded
or a Button Battery intended for Solar Powered Wallet (Credit Card Sized) Calculators.
A
B
-110.712G
-110.712G
SJ20
SJ21
RotorLoad5
10m H
SJ22
SJ23
RotorLoad6
10m H
SJ24
SJ25
RotorLoad7
10m H
SJ26
SJ27
RotorLoad8
10m H
SJ28
SJ29
RotorLoad9
10m H
C
D
-110.712G
-110.712G
SJ31
Nine rotor loads, connected in parallel, is the maximum before gain becomes a loss.
Simulation Max Time Step is Zero
Magnetic Couplings #2
Armature1 StackOfAluminumDisks
Armature2 StackOfAluminumDisks
Magnetic Couplings #3
StatorLoad StackOfAluminumDisks
CopperWireCageForTheAluminumDisks StackOfAluminumDisks
Magnetic Coupling #1
StatorLoad Armature1 Armature2 CopperWireCageForTheAluminumDisks
Magnetic Coupling #4
StatorLoad RotorLoad1 RotorLoad2 RotorLoad3 RotorLoad4 RotorLoad5 RotorLoad6 RotorLoad7 RotorLoad8 RotorLoad9


Transient Analysis Limits
Run
Add
Delete
Expand...
Stepping...
PSS...
Properties...
Help...
Maximum Run Time
3.0000000000001e5
Output Start Time (tstart)
38k
Maximum Time Step
0
Number of Points
51
Temperature
Linear
27
Retrace Runs
1
Run Options
Normal
State Variables
Zero
Operating Point
Operating Point Only
Auto Scale Ranges
Accumulate Plots
Fixed Time Step
Periodic Steady State
Ignore Expression Errors
P..
P
X
Y Expression
X Range
Y Range
I(C3)
RMS(V(SolarPanel))
RMS(V(CDS))
RMS(V(CDL))
RMS(I(SolarPanel))
RMS(I(CDS))
RMS(I(CDL))
RMS(V(StatorLoad))
RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9))
RMS(I(StatorLoad))
RMS(I(RotorLoad1))+RMS(I(RotorLoad2))+RMS(I(RotorLoad3))+RMS(I(RotorLoad4))+RMS(I(RotorLoad5))+RMS(I(RotorLoad6))+RMS(I(RotorLoad7))+RMS(I(RotorLoad8))+RMS(I(RotorLoad9))
RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9))
RMS(I(StatorLoad))+RMS(I(RotorLoad1))+RMS(I(RotorLoad2))+RMS(I(RotorLoad3))+RMS(I(RotorLoad4))+RMS(I(RotorLoad5))+RMS(I(RotorLoad6))+RMS(I(RotorLoad7))+RMS(I(RotorLoad8))+RMS(I(RotorLoad9))
(RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9)))*(RMS(I(Stator
(RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9)))/(RMS(I(Stator
V(Armature1)
I(Armature1)
V(StackOfAluminumDisks)
I(StackOfAluminumDisks)
autoalways


now7a3d, 70pc reduction of armature and zero max time step.cir
1.51
1.51
1.51
1.50
1.50
1.50
38.00K
52.40K
104.80K
157.20K
209.60K
262.00K
300.00K
RMS(V(SolarPanel))
RMS(V(CDS))
1.65
1.50
1.35
1.20
1.05
0.90
RMS(V(CDL))
RMS(I(CDL))
1.01u
1.01u
1.00u
1.00u
1.00u
RMS(I(SolarPanel))
RMS(I(CDS))
135.00
120.00
105.00
90.00
75.00
60.00
RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9))
40.00
36.00
32.00
28.00
24.00
20.00
RMS(I(StatorLoad))+RMS(I(RotorLoad1))+RMS(I(RotorLoad2))+RMS(I(RotorLoad3))+RMS(I(RotorLoad4))+RMS(I(RotorLoad5))+RMS(I(RotorLoad6))+RMS(I(RotorLoad7))+RMS(I(RotorLoad8))+RMS(I(RotorLoad9))
5.25K
4.50K
3.75K
3.00K
2.25K
1.50K
(RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9)))*(RMS(I(StatorLoad))+RMS(I(RotorLoad1))+RMS(I(R
3.09
3.09
3.09
3.09
3.09
(RMS(V(StatorLoad))+RMS(V(RotorLoad1))+RMS(V(RotorLoad2))+RMS(V(RotorLoad3))+RMS(V(RotorLoad4))+RMS(V(RotorLoad5))+RMS(V(RotorLoad6))+RMS(V(RotorLoad7))+RMS(V(RotorLoad8))+RMS(V(RotorLoad9)))/(RMS(I(StatorLoad))+RMS(I(RotorLoad1))+RMS(I(Rc
T (Secs)



The last chart of a black line at the bottom of a numeric readout portrays the impedance, namely: the ratio of voltage to current, as being approximately 3.09 so that the voltage at the termination of this analysis is three times the current; or, 110.6 volts versus 35.8 & a third amps.

I hope you have enjoyed this trip down fantasy lane! Who knows? Maybe these circuits are buildable? Then again, maybe they're not!

;-)